



Indicators of reproducibility and suitability for assessing the quality of production services

Oleksandr Vasilevskyi¹, Maryna Koval¹, Svetlana Kravets²

¹ Vinnytsia National Technical University, 95 Khmelnitsky Shose str., 21021 Vinnytsia, Ukraine

² Vinnytsia National Agrarian University, 3 Solnyschna St., 21008 Vinnytsia, Ukraine

ABSTRACT

A technique is proposed for estimating the probability of the possible appearance of defective products or the inconsistency of the production service on the basis of indexes of suitability and reproducibility of the production process. The index of reproduction is recommended to be calculated on the basis of the standard deviation, which can be established by the average span of the control map and the limits of the tolerance field. At the same time, the production process must necessarily be in a state of statistical controllability. The suitability index cannot be calculated on the basis of the control card characteristics, but it is evaluated solely on the basis of the total of the standard deviation, which is calculated by the Bessel formula and the tolerance limits. The production process does not need to be statistically controllable. Conclusions on the suitability or insufficiency of the products (production services) are based on the value of the indexes of reproduction and suitability, which can take values less than or greater than one. On the basis of these indexes of obtained values, the probability of production appearance or characteristics of the production process, that does not match the established requirements, is established.

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Keywords: Quality assessment; product quality; quality of manufacturing services; suitability index; reproducibility index; probability of defective product, production process

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Corresponding author: Oleksandr Vasilevskyi, e-mail: o.vasilevskyi@gmail.com

1. INTRODUCTION

To ensure the competitiveness of enterprises products, manufacturers should apply a strategy of continuous improvement. For the implementation of a such strategy, product manufacturers or service providers need to constantly evaluate their products [1]. It is advisable to apply the methods recommended by the international standards of the ISO / TR 18532, ISO 13528 and ISO / TR 22514 [2]-[5]. For the successful implementation of actions to continually improve the quality of products or services, it is necessary to monitor the sources of the production process deviations and their stability. In the conditions of competition for producers, not only the price of products or services should be important, but also the costs, that consumers will spend when using products (or services). Therefore, the purpose of any manufacturer should be to

continuously reduce the deviations of the production process parameters (ensuring the stability of the production process), and not only compliance with established requirements. The strategy of continuous improvement will reduce the costs associated with failures, and will increase the sustainability of enterprise development in a competitive environment. In addition, reducing deviations will reduce control costs or reduce the frequency of selective control. Quantitative evaluation of deviations allows us to make conclusions about the suitability and conformity of the production process to the established requirements. For identification of deviations, the different methods, such as drawing up a flowchart and identifying inputs and outputs of a production process, using a causal diagram, etc. can be used.

A number of international standards [1]-[7] recommend a variety of statistical methods that can be used to manage, control

and improve the production process in order to analyze data and evaluate product quality indicators.

Therefore, the purpose of this article is to develop mathematical models for point estimation of reproducibility indices and the suitability of the production process to confirm its statistical stability, as well as to determine the fraction of the probability of defective products. The description of the mathematical models that can be used to evaluate the quality indexes on the basis of reproduction and suitability indexes is an actual scientific task, since many manufacturers of products do not understand their differences and consequently incorrectly interpret the obtained results.

2. MATERIALS AND METHODS

The first step requires to develop methods for evaluating the quality indexes of products (services) on the basis of the indexes of reproducibility and suitability of the production process, as well as to formulate the criteria for normalization of reproduction and suitability indexes for decision-making on conformity (sufficient, satisfactory, good) or noncompliance of product quality indicators or production services to the established requirements.

The article reviews the methodology for calculating the reproducibility level of product production, depending on the input data set. Depending on the specifics of production and the adopted quality management strategy, we may have a specific set of data to calculate the value of reproducibility. Therefore, one unified methodology cannot be adopted because it may give erroneous results. The level of production reproducibility is a very important element in the process efficiency assessment process according to the Deming cycle. Based on the statistical calculations made and review of the methodologies included in the literature, the assessment approach was optimized depending on the possibility of obtaining data recorded during production.

When analyzing the reproducibility of the production process, it is necessary (ISO 5725:2002) [7]:

- a) establish all requirements of the production environment (e.g. temperature and humidity requirements);
- b) establish requirements for uncertainty of measurements;
- c) ensure an opportunity to analyze multifactor, multilevel aspects of the production process;
- d) establish and register the length of data receiving;
- e) determine the frequency of sample creation, as well as the start and end date of the data receiving;
- f) use a control card to control the production process [8];
- g) to provide the state of statistical control of the production process.

Indicator of the reproducibility of a production process is a measure of its own change of the output characteristics of the production process, which is in a state of statistical control, and which enables to assess the ability of the process to maintain the output characteristics of the production process at the level of requirements set for it. This measure characterizes the variability that remains after eliminating all known causes. If the control of the production process is carried out using a control card, then the control card shows that the production process is in a controlled state [4], [8]-[10]. Reproducibility of the production process is often estimated by the number of products, the characteristics of which are within the tolerance field. Since the production process in a statistically controlled state can be described by the predicted distribution law, then the quantity of products which characteristics is beyond the tolerance field can

Table 1. Coefficients of the control card to estimate the standard deviation.

Sample size (n)	d_2	c_4
2	1.128	0.7979
3	1.693	0.8862
4	2.059	0.9213
5	2.326	0.9400
6	2.534	0.9515
7	2.704	0.9594
8	2.847	0.9650
9	2.970	0.9693
10	3.078	0.9727

be estimated. While the production process remains in a state of statistical control, the manufactured products have, on average, the same proportion of the defective products (products that do not match the established requirements).

The actions of the production process management, which are aimed to reducing the deviations caused by accidental causes, will make it possible to improve the conformity of the production process with the requirements of the quality management system [10]. To do this, it is necessary: to determine the characteristics of the production process and the conditions of operation (if the conditions are changed, then new studies of the characteristics of the production process are necessary); to evaluate the parameters of short-term and long-term deviations in the form of percentages from full changes and to minimize them; maintain the stability of the production process and ensure its statistical control; to evaluate the own variability of the reproduction process; select the required parameter of the reproducibility of the production process.

Also, it is necessary to check the control card, the data of which had been used for statistical control, and the histogram data with all the established limits applied to it. In addition, it is necessary to check the normality of the distribution law by a valid criteria, for example, such as the Anderson-Darling criteria [10] or the χ^2 -criteria [4]. These criteria are effective in detecting the deviation of the law of distribution from normality on the distribution tails, since this area is important in the evaluation of the indexes of reproduction and suitability of the production process. Also, an abnormal data explanation must be found and appropriate actions taken with the data to calculate the investigated parameter. Exclusion of data allocated to others is unacceptable. Such deviations can be very informative about the properties of the production process and should be investigated.

Reproducibility parameter of the production process may be a value that characterizes one or more properties of the distribution of the input characteristic in the conditions of the production process reproducibility. The general parameter of the distribution position is the mean (mathematical expectation) μ , but sometimes selective median $X_{50\%}$ is used. For a normal distribution law, the best position parameter is the median.

The best parameter characterizing the own variability of the production process is the standard deviation σ - index of reproducibility of the production process. It is recommended to evaluate it according to the average magnitude \bar{R} obtained by the control card, when the production process is stable and is in a state of statistical control

$$\hat{\sigma} = \frac{\bar{R}}{d_2}, \quad (1)$$

where d_2 is a constant corresponding to the sample size in the subgroup, its value is chosen from Table 1 [9].

If we use the average standard deviation for controlling deviations within a subgroup, which is determined by the data of the control card, then the own standard deviation of the production process can be estimated by the formula

$$\hat{\sigma} = \frac{\bar{S}}{c_4}, \quad (2)$$

where \bar{S} is the average sampled standard deviation and c_4 the constant corresponding to the sample size in the subgroup (n); its value is chosen from Table 1 [9].

If for each subgroup it is possible to calculate the standard deviation of a subgroup, then a formula for assessing the standard deviation of the production process is recommended, which gives a more accurate estimate than formulas (1) and (2), which is described by formula

$$\hat{\sigma} = \sqrt{\frac{1}{m} \sum_{j=1}^m S_j^2}, \quad (3)$$

where S_j is the sampled standard deviation of j -th subgroup; m - is the number of subgroups with n observations in each subgroup.

It is also necessary to distinguish between the standard deviation, that characterizes only short-term changes in the production process, and the standard deviation that characterizes the long-term changes in the production process. And the data received over a long period of time have bigger value of standard deviation due to a more significant change in the production process. In this case, it is recommended to use the symbol σ_t to denote the standard deviation - the total (full) standard deviation.

If the data are obtained from the observation of a production process that is not in a state of statistical control or if control cards have not been used, then formula (1) - (3) should not be used to calculate the standard deviation, but it is necessary to apply the following formula:

$$\hat{\sigma}_t = \sqrt{\frac{1}{N-1} \sum_{i=1}^N (x_i - \bar{x})^2}, \quad (4)$$

where N is the total sample size, x_i the i -th value in the sample, \bar{x} the average arithmetic mean.

Equation (4) should be used when the production process has a change in the average value due to the presence of a systematic error [11]-[13], which can not be excluded, and this variability must be taken into account with along the random variability. This variation parameter is also suitable for use in the calculation of the suitability indexes of the production process.

With the normal distribution of the production process as an estimate of the reproducibility of the production process, an expression can be used

$$\bar{x} \pm z_\alpha \cdot \hat{\sigma}_t, \quad (5)$$

where $\bar{x} = \frac{1}{m} \sum_{j=1}^m \bar{x}_j$ is the arithmetic average of several sample meanings; \bar{x}_j the selective average of j -th subgroup; z_α a quantile of a normalized normal distribution law.

The choice of the value of z_α depends on the used value of the reproducibility index of the production process in units of production of one million. Typically, z_α is assigned a value of 3, 4 or 5. If the reproducibility index of the production process

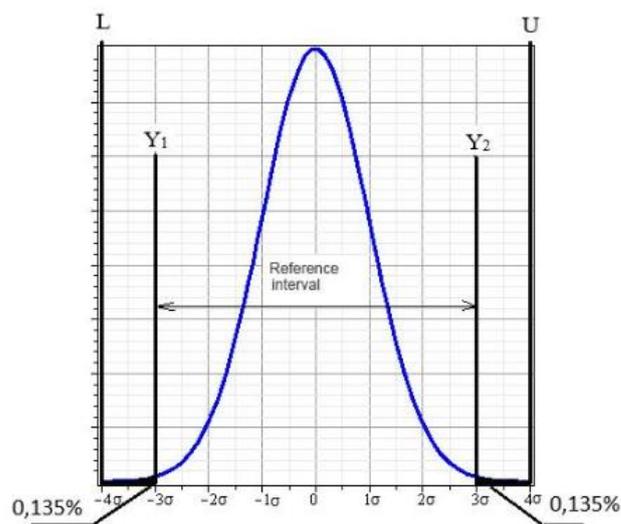


Figure 1. The length of the reference interval T and the lower L and the upper U limits of the tolerance field.

matches the requirements, $z_\alpha = 3$ means an average of 2700 units of products per million beyond the requirements. Similarly, $z_\alpha = 4$ means an average of 64 units of products per million that do not match the established requirements, and $z_\alpha = 5$ means an average of 0.6 such items per million.

Reproducibility indexes of the production process are the point of estimation of their reference values. Using the reproducibility index of the production process allows us to characterize the state of the production process. The index of reproducibility of the production process is the ratio between the differences of the tolerance field to the length of reference interval

$$C_p = (U - L) / (X_{99,865\%} - X_{0,135\%}), \quad (6)$$

where L is the lower limit of the tolerance field; U the upper limit of the tolerance field; $X_{0,135\%}$ the lower limit of the reference interval defined as the quantile of distribution at the level of 0,135%; $X_{99,865\%}$ the upper limit of the reference interval, which is defined as quantile of distribution at 99,865%.

To estimate the index of reproducibility of the production process the reference interval $T = Y_2 - Y_1$ is used [4], [5], which includes 99.73% of the production process characteristics values, which are in the state of statistical control. At the same time 0.135% of each side of the distribution law is cut off [13], [14]. This interval is recommended to apply even in the case of a non-normal distribution law of the production process characteristics values [13]. For a normal distribution law, the length of the reference interval is six standard deviations (Figure 1).

Control maps are usually used to evaluate reproducibility. If the control card shows weakened control lines or modified control lines, the actual standard deviation of the process will be greater than the standard deviation obtained from the control card with standard control lines. These features affect the reference interval, so it is important that the standard control lines were fixed in the evaluation of the reproducibility index of the production process.

A reproducible process is a production process with a reference interval T smaller than the tolerance field (L, U) for a certain value, as shown in Figure 1.

It is also recommended by international standards [1], [3], [4] to use other indexes that characterize both the state and the

variability of the production process, for example, the reproducibility index C_{P_k} . If this index is smaller than a given value, then it can be assumed that in the manufacturing process there is a high probability of occurrence of defective products, that is, the characteristic of the production process goes beyond the tolerance field (L, U).

The reproducibility indexes C_{P_k} can be defined as the ratio of difference between the tolerance field and the production process value to the difference between the corresponding limits of the production process value and the parameter of the production process:

$$C_{P_{kU}} = (U - X_{50\%}) / (X_{99,865\%} - X_{50\%}), \quad (7)$$

$$C_{P_{kL}} = (X_{50\%} - L) / (X_{50\%} - X_{0,135\%}), \quad (8)$$

where $X_{50\%}$ is the quantile of the distribution law of the production process at the level of 50%.

These reproducibility indexes ($C_{P_{kL}}$) provide information about how tightly the characteristics are grouped around the centerline and whether product specification requirements may be violated.

Even if the value of the index C_p , $C_{P_{kU}}$ is high, then the low values of the C_{P_k} indexes indicate that the production process is poorly concentrated around the central line, and the probability of the appearance of quality characteristics values beyond the established limits of the set requirements is high.

If the observed values are distributed according to the normal distribution law, the length of the reference interval is equal to 6σ , and the reproducibility index can be estimated by expression

$$\hat{C}_p = (U - L) / (6\hat{\sigma}). \quad (9)$$

If the distribution of individual values is subject to the normal distribution law, then quantile $X_{50\%}$ is equal to the mathematical expectation μ , and the upper and lower indexes of the reproducibility C_{P_k} can be estimated from the expressions:

$$\hat{C}_{P_{kU}} = (U - \mu) / (3\hat{\sigma}), \quad (10)$$

$$\hat{C}_{P_{kL}} = (\mu - L) / (3\hat{\sigma}). \quad (11)$$

Based on the evaluation of the lower $\hat{C}_{P_{kL}}$ and upper $\hat{C}_{P_{kU}}$ reproducibility indexes, for the final evaluation of the reproducibility index C_{P_k} , it is necessary to assume a lower reproducibility index

$$\hat{C}_{P_k} = \min(\hat{C}_{P_{kL}}, \hat{C}_{P_{kU}}). \quad (12)$$

In calculating the reproducibility index of the production process, it must be taken into account that the variability of the production process should correspond to the situation when the data has been obtained in a state of statistical control of the production process.

3. EMPIRICAL RESULTS

If the index of the reproducibility $C_p < 1$ (or $C_{P_k} < 1$), then the upper U and the lower L limits of the tolerance field are inside the reference interval T of the production process - this means that the production is not possible without a defect, and the production process is unsatisfactory (the probability of defective production is very high and may be higher than 0.27%).

If the value $C_p = 1$ (or $C_{P_k} = 1$), then the upper U and the lower L limits of the tolerance field coincide with the reference interval T of the production process. In this case, if the process

is centered and the distribution of quality indicators obeys the normal law, then the possible lack of products is 0.27% (2700 defective products per 1 million manufactured goods). In this case, the production process is considered to be the minimum acceptable (satisfactory, it is recognized as reproducible).

If the value of the reproducibility index $C_p > 1$ (or $C_{P_k} > 1$), then the upper U and the lower L limits of the tolerance field are outside the reference interval T of the manufacturing process - this means that production is possible without defects, and the production process is considered to be satisfactory. If the value C_{P_k} (or C_p) lies within $1 < C_{P_k} < 1.33$, then the probability of occurrence of defective products will be in the range from 0.006% to 0.27%. If the value of the index of reproducibility is greater than 1.33 ($C_{P_k} > 1.33$), then the probability of occurrence of defective products is less than 0.006%, and the production process is considered good.

The appropriateness of the production process regarding the quality of products is the achieved distribution of results.

The only important difference between the suitability and reproducibility of the production process is that for assessing the suitability of the production process there is no requirement for the presence in the production process of the state of statistical control and control cards.

In the analysis of the suitability of the production process:

- all technical conditions, including requirements for the production environment, such as temperature and humidity requirements, must be established [8], [15];
- requirements for uncertainty of measurements must be established [15]-[24];
- an opportunity should be provided for the analysis of multi-factor and multilevel aspects of the production process;
- data must be obtained and registered within a specified time period;
- the frequency of sampling and the start and end of time of the data obtaining must match the requirements set by the quality management system [1];
- the process may not be monitored by a control card;
- the process may be statistically uncontrolled, in particular, previously obtained data, which sequence is unknown, can be used to assess the suitability of the production process.

The index of the suitability of the production process is a statistical indicator, which is determined by the output characteristic of the production process, which used to evaluate the production process, the location of which in the state of statistical control is not confirmed. The parameter of the suitability of the production process may be the quantities describing one or more properties of the quality characteristic distribution in terms of suitability. To estimate the suitability parameter, in contrast to the reproducibility parameter, under the normal distribution of the quality characteristic, we can only by expression (4). The index of the suitability of a production process is an index that reflects the stability of the production process to the specified field of tolerance.

If the values of the parameters under study are distributed according to the normal distribution law, then the length of the reference interval is equal to $6\hat{\sigma}_t$ [25], [26]. Therefore, the value of the index of fitness P_p can be calculated by expression

$$P_p = (U - L) / (6\hat{\sigma}_t). \quad (13)$$

The upper $P_{P_{kU}}$ and lower $P_{P_{kL}}$ indexes of the suitability of the production process can be estimated by the expressions:

$$P_{pkU} = (U - \bar{x}) / (3 \hat{\sigma}_t), \quad (14)$$

$$P_{pkL} = (\bar{x} - L) / (3 \hat{\sigma}_t). \quad (15)$$

The indexes of the suitability of the production process P_{pk} is assumed to be equal to the lower of the two values of P_{pkU} and P_{pkL} , i.e. $P_{pk} = \min(P_{pkU}, P_{pkL})$. The lower the value of the index of suitability, the greater the probability of occurrence of defective products, and the production process will not match the established requirements.

As follows from expressions (13) - (15), the assessment of the indexes of suitability is similar to the evaluation of reproducibility indexes (6) - (12). The difference in the evaluation of suitability indexes from the reproducibility indices is that the production process does not necessarily have to be statistically controlled, and the standard deviation that characterizes the best indicator of the suitability of the production process can not be calculated based on the parameters of the control card.

The P_{pk} suitability index characterizes the confirmed quality. If the production process is centered, that P_{pk} , but when the process is shifted, the suitability index is shifted from its nominal value, and $P_{pk} = P_p$ becomes less than P_p index will only be the case when the goal is achieved with a minimum deviation from the average arithmetic value.

In case of noncentration of the production process, the P_p index can be adjusted by introducing a noncentral correction

$$P_{pk} = (1 - k)P_p, \quad (16)$$

where k is a corrective coefficient that corresponds to the value of noncentration and is defined as the difference between the given reference value of the product characteristic and the average value of the production process parameter.

If the process is centered, then $k = 0$ and P_{pk} . If the process is shifted relative to a given reference value, then k increases and the index $P_{pk} = P_p$ becomes smaller than the P_p index.

If the suitability indexes are equal to ($P_{pk} = P_p$), the production process is within the tolerance. If the index $P_p < 1$, then this means that the production process has low accuracy and the production process is unsatisfactory. The using of statistical methods [3]-[7] during the regulation will not give the necessary effect. In this case, it is necessary to improve the accuracy of the production process by replacing (or/and repairing) technical equipment and ensuring the quality of measurements (unity of measurements and accuracy of measurements) [25].

If the P_{pk} suitability index is in the range from 1 to 1,33 ($1 \leq P_{pk} < 1,33$), the production process has sufficient accuracy - this means that the procedure for setting it up is correct. At the same time it is advisable to apply the acceptance control cards and to combine the procedure of manufacturing process regulation and the acceptance of products in one common procedure of the SPC (Statistical Process Control) [25]-[28].

If the index $P_p > 1,33$, then the production process is considered to be good (with high potential accuracy).

If $P_p > 1$ and $P_{pk} < 1$, then the production process is considered to have sufficient potential precision, but there are factors that shift the manufacturing process and remain unnoticed. In this case, it is recommended to use Shuhart's control cards to identify factors that may result in displacement of the manufacturing process center.

If the index $P_p > 1,66$, then the production process is ideally configured [28].

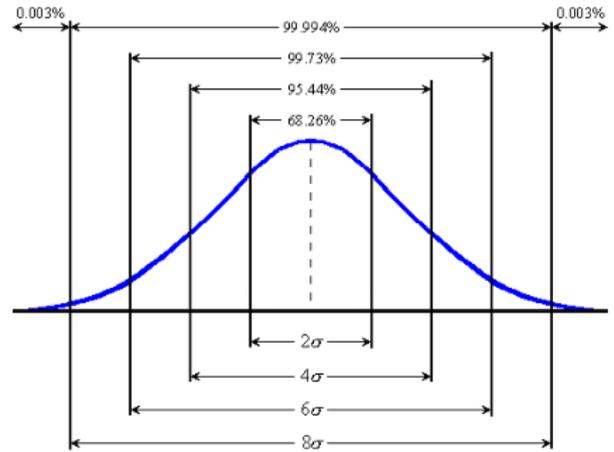


Figure 2. Properties of the normal distribution law, on which the calculation of the defect fraction is based.

The main properties of the normal distribution law, on which the calculation of the defect fraction is based, are shown in Figure 2.

As it follows from Figure 2, in order to avoid a noticeable fraction of defective products or characteristics of the production process that deviates from the established requirements, the width of the tolerance field must be not less than 6σ .

Estimation of the values of p_t production process characteristic or the quality parameter of products that do not match the requirements under the normal distribution law can be found on the basis of the upper and lower parts of units that do not match the requirements:

$$\hat{p}_t = \hat{p}_L + \hat{p}_U = \Phi\left(\frac{L - \bar{x}}{\hat{\sigma}_t}\right) + \Phi\left(\frac{\bar{x} - U}{\hat{\sigma}_t}\right), \quad (17)$$

$$\hat{p}_L = 1 - \Phi(3 \hat{C}_{pkL}), \quad (18)$$

$$\hat{p}_U = 1 - \Phi(3 \hat{C}_{pkU}), \quad (19)$$

where \hat{p}_L is the assessment of the lower part of the units that do not match the requirements - the part of units of the process or product characteristics distribution, which does not exceed the lower limit of the field of tolerance L ; \hat{p}_U is the assessment of the upper part of the units that do not match the requirements - the part of units of the process or product characteristics distribution, that exceeds the upper limit of the tolerance field U ; $\Phi(*)$ - the function of a normalized normal distribution law.

In order to estimate the proportion of product units that do not match the requirements of the suitability of the production process, it is necessary to replace the reproducibility indexes and indexes of suitability in formulas (18) and (19), and thus common part of the values of the characteristics distribution of the production services (production process) that may go beyond the tolerance field.

4. MEASUREMENT SYSTEMS ANALYSIS

Measurement systems analysis (MSA) [5], [29] manual presents guidelines for assessing the quality of a measurement system primarily used in the industrial world. Three fundamental issues must be addressed when evaluating a measurement system: the measurement system must demonstrate adequate resolution to detect changes in product or process variation.

Typically, its applied that instrument discrimination should divide the tolerance (or process variation) into ten parts or more; the measurement system must be stable. Under repeatability conditions, the measurement system variation is due to common causes only and not special causes; the statistical properties (errors) are consistent over the expected range and adequate for the purpose of measurement (product control or process control).

The location characteristics are defined by Bias (systematic error component of the measurement system), linearity (the change in bias over measuring range) and stability (the change in bias over time).

Repeatability and reproducibility are considered for variation characteristics (Figure 1). Gage repeatability and reproducibility standard-deviation (GRR) is the combined estimate of measurement system repeatability and reproducibility. GRR percentile calculation (%GRR) when compared to the product tolerance (T), is calculated according to equation:

$$\%GRR = \frac{6 \cdot \hat{\sigma}_t}{T} 100 \%, \quad (20)$$

where $T = Y_2 - Y_1$ is the product tolerance.

Table 2 presents a summary of the acceptance criteria set out in the 4th edition of MSA manual [25], [30]. The analysis of these parameters is relevant only if the measurement system is stable. For Bias and linearity characteristics, they are required to be significantly equal to zero for a 95% confidence level, and the errors obtained in experiments should be less than the maximum permissible errors established for the instruments. This requirement considers that systematic errors should be practically non-existent, presenting only random errors. However, it is common for equipment to remain repetitive, but with typical systematic errors. But, when compared with the product tolerance, it represents a small portion.

For the variation characteristic of a measurement system, the acceptance criteria is 10 % of the tolerance or variation of the production process. The change in this last revision of MSA manual is that, depending on the application or the costs involved, values up to 30 % for %GRR could be acceptable, but it must be approved by the client. The conformity assessment consists of verifying compliance with product tolerance, established between lower specification limit (LSL) and higher specification limit (USL). Usually, decisions about compliance with the requirement depend on the measures obtained in the product inspection. Since the decisions are made according measurement results, and these measurements are characterized by uncertainty, these decisions may be incorrect [30], [31]. Such incorrect decisions are of two types: an item accepted as conforming may actually be nonconforming, and an item rejected as non-conforming may actually be conforming.

Table 2. Acceptance criteria established in MSA manual.

Characteristic	Acceptability criteria
Bias and linearity	In general, significantly equal to zero and not exceed the maximum permissible error established by the gage calibration.
%GRR	<10% tolerance (or process variation): Generally considered to be an acceptable measurement system. 10–30% tolerance (or process variation): May be acceptable for some applications, but should be approved by the customer.

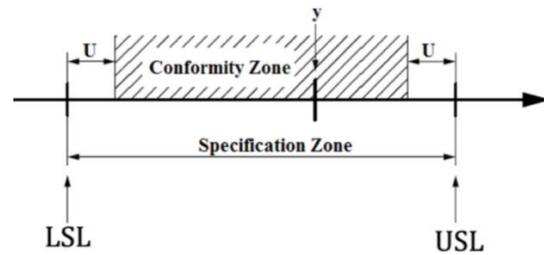


Figure 3. Conformity with specification.

According to ISO 14253-1 [32], if no previous agreement has been made between the supplier and the customer, the principle behind the rules for proving conformity and nonconformity with specifications is the following: the measurement uncertainty always counts against the party who is providing the proof of conformity or nonconformity and therefore making the measurement. The supplier shall prove conformity with a specification. It is proved when the complete measurement result (including measurement uncertainty) falls within the tolerance zone of a workpiece characteristic (Figure 3). And the customer shall prove nonconformity with a specification to could prove a product. Nonconformity with a specification is proved when the complete measurement result falls outside the tolerance zone.

Regions reduced or extended to the tolerance field are called guard bands U (Figure 3).

JCGM 106 [33] points out that the use of these guard bands (U) provides a way to limit the probability of making an incorrect conformance decision based on measurement information. JCGM 106 also lists the rule known as shared risk [31]. Under this rule, the customer and supplier agree to accept as conforming (and reject otherwise) an item whose property has a measured value in the tolerance interval. In this case, producer and user share the consequences of incorrect decisions. And a limit for the measurement uncertainty must be established.

In the MSA manual, the parameter related to the measurement uncertainty is $\hat{\sigma}_t$, where $6 \cdot \hat{\sigma}_t$ represents the variation of the measurement system to a confidence level of 99,73 %. In its most rigorous condition, %GRR cannot be greater than 10% of tolerance and Bias should be significantly equal to zero. If there is an agreement with the customer, %GRR could reach 30% of tolerance.

The standard-deviation of the real productive process $\hat{\sigma}_{rpp}$ is obtained by equation (11), where $\hat{\sigma}_t$ is the measured standard-deviation of the manufacturing process, $\hat{\sigma}_{mp}$ is the standard-deviation of the measurement process

$$\hat{\sigma}_{rpp}^2 = \hat{\sigma}_t^2 - \hat{\sigma}_{mp}^2. \quad (21)$$

Measurement systems must be adequate for the required measurement task, and statistical studies should be performed to assess the impact of measurement uncertainty on the manufacturing process. However, care must be taken not to disable appropriate measuring systems due to the use of overestimated acceptance criteria.

5. CONCLUSIONS

The quality of products or services is largely determined by the effectiveness of the quality management system at the enterprise and the proper organization of the production process. The quality management system, built in accordance with the principles of overall quality management, involves continuous improvement of the marketing activities of the

enterprise, improving the quality of products and ensuring of the needs of all interested parties, both customers and producers, through the establishment of appropriate management in the enterprise.

The application of indexes of reproducibility and suitability of the production process in the system of quality control allows us to visually estimate the possibility of reducing the percentage of defective products by reducing and eliminating the effects of non-random causes of the production process parameters deviation (ensuring the stability of the production process), as well as reducing the impact of the random reasons leading to deviations of the production process parameters. This will allow timely warning and corrective actions that will enable them to find reserves for improving product quality, reduce financial costs for defective repair, and increase the competitiveness of the enterprise.

The reproducibility index and suitability index are not related to the mean of the process. That is, when the entire distribution is shifted, the reproducibility index and the fitness index will not change, it will only respond to the variation of the spread or sweep. The reproducibility index and the suitability index will be equal to 1 when the variation of 6σ is equal to the tolerance. If the indices are greater than 1, then the range is less than the tolerance, if the indices are less than 1, then the variation is greater than the tolerance. It should be taken into account that since the indices are not related to the position of the mean, then when the mean is far beyond the tolerance, the value of the indices may be much greater than 1.

The accuracy of the proposed estimation methodology of the reproducibility and suitability index, which includes the proposed mathematical apparatus, was estimated on the basis of the correctness index, the method of assessment of which is carried out in accordance with the international standard ISO 57252:2002.

In conditions requiring a high degree of accuracy (or not), acceptance criteria would be agreed directly between customers and suppliers. That is, it would be up to the client to specify items that require more stringent acceptance criteria. Only in extraordinary situations, it would be up to the supplier to demonstrate that a measurement system with the highest measurement error still performs measurement task correctly, whether due to the high capability of the manufacturing process or due to the use of guard bands.

REFERENCES

- [1] ISO, Quality management systems - Fundamentals and vocabulary, ISO 9000:2015 (2015).
- [2] ISO/TR, Guidance on the application of statistical methods to quality and to industrial standardization, ISO/TR 18532:2009 (2009).
- [3] ISO, Statistical methods in process management - Capability and performance - part 2: process capability and performance of time-dependent process models, ISO 22514-2:2017 (2017).
- [4] ISO/TR, Statistical methods in process management - Capability and performance - part 4: process capability estimates and performance measures, ISO/TR 22514-4:2016 (2016).
- [5] ISO, Statistical methods for use in proficiency testing by interlaboratory comparisons, ISO 13528:2015 (2015).
- [6] ISO, Statistical control. Selective control on alternative grounds - part 5: continuous sampling plan systems, indexed by quality assurance limits (MPY) for consecutive sampling of parties, ISO 2859-5: 2009 (2009).
- [7] ISO, Accuracy (trueness and precision) of measurement methods and results - part 2: basic method for the determination of repeatability and reproducibility of a standard measurement method, ISO 5725-2:2002 (2002).
- [8] B. Ristic, J. Houssineau, S. Arulampalam, Robust target motion analysis using the possibility particle filter, *IET Radar Sonar Navigation* 13(1) (2018) pp. 18-22.
DOI: [10.1049/iet-rsn.2018.5144](https://doi.org/10.1049/iet-rsn.2018.5144)
- [9] O. M. Vasilevskiy, M. M. Koval, A comprehensive approach to the qualimetric assessment of indicators quality of products, *Perspective trajectory of scientific research in technical sciences, collective monograph*, Riga: Izdevnieciba "Baltija Publishing" (2021) pp. 62-85.
DOI: [10.30525/978-9934-26-085-8-4](https://doi.org/10.30525/978-9934-26-085-8-4)
- [10] A. Antonucci, C. P. de Campos, D. Huber, M. Zaffalon, Approximate credal network updating by linear programming with applications to decision making, *Int. J. Approx. Reason* 58(3) (2014) pp. 25-38.
DOI: [10.1016/j.ijar.2014.10.003](https://doi.org/10.1016/j.ijar.2014.10.003)
- [11] Carlos Mauricio Villamizar Mora, Jonathan Javier Duarte Franco, Victor Jose Manrique Moreno, Carlos Eduardo García Sánchez, Analysis of the mathematical modelling of a static expansion system, *Acta IMEKO* 10(3) (2021) pp. 185-191.
DOI: [10.21014/acta_imeko.v10i3.1061](https://doi.org/10.21014/acta_imeko.v10i3.1061)
- [12] Oleksandr Vasilevskiy, Assessing the level of confidence for expressing extended uncertainty through control errors on the example of a model of a means of measuring ion activity, *Acta IMEKO* 10(2) (2021) pp. 199-203.
DOI: [10.21014/acta_imeko.v10i2.810](https://doi.org/10.21014/acta_imeko.v10i2.810)
- [13] W. Anderson, Anderson-Darling Test for Goodness-of-Fit, *Int. Encyclopedia of Statistical Sciences* (2011).
DOI: [10.1007/978-3-642-04898-2_118](https://doi.org/10.1007/978-3-642-04898-2_118)
- [14] B. Fortin, S. Hachour, F. Delmotte, Multi-target PHD tracking and classification using imprecise likelihoods, *Int. J. Approx. Reason* 90 (2017) pp. 17-36.
DOI: [10.1016/j.ijar.2017.06.013](https://doi.org/10.1016/j.ijar.2017.06.013)
- [15] D. J. Wheeler, An Honest Gauge R&R Study, 189 (2009). Online [Accessed 04 December 2021]
<http://www.spcpress.com/pdf/DJW189.pdf>
- [16] Sueli Fischer Beckert and Wagner Saucedo Paim, Critical analysis of the acceptance criteria used in measurement systems evaluation, *International Journal of Metrology and Quality Engineering* 8(23) (2017), art. no. 23.
DOI: [10.1051/ijmqe/2017016](https://doi.org/10.1051/ijmqe/2017016)
- [17] O. M. Vasilevskiy, Calibration method to assess the accuracy of measurement devices using the theory of uncertainty, *Int. J. Metrol. Qual. Eng.* 5(4) (2014), art. no. 403.
DOI: [10.1051/ijmqe/2014017](https://doi.org/10.1051/ijmqe/2014017)
- [18] Francesco Lamonaca, Domenico Luca Carni, Domenico Grimaldi, Time coordination of standalone measurement instruments by synchronized triggering, *Acta IMEKO* 4(3) (2015) pp. 23-29.
DOI: [10.21014/acta_imeko.v4i3.259](https://doi.org/10.21014/acta_imeko.v4i3.259)
- [19] O. Vasilevskiy, V. Didych, A. Kravchenko, M. Yakovlev, I. Andrikevych, D. Kompanets, Y. Danylyuk, W. Wojcik, A. Nurmakhambetov, Method of evaluating the level of confidence based on metrological risks for determining the coverage factor in the concept of uncertainty, *Proceedings Volume 10808, Photonics Applications in Astronomy, Communications, Industry, and High-Energy Physics Experiments 2018*, 108082C.
DOI: [10.1117/12.2501576](https://doi.org/10.1117/12.2501576)
- [20] ISO/IEC, General requirements for the competence of testing and calibration laboratories, ISO/IEC 17025:2005 (2005).
- [21] O. M. Vasilevskiy, Metrological characteristics of the torque measurement of electric motors, *Int. J. Metrol. Qual. Eng.* 8 (7) (2017), art. no. 7
DOI: [10.1051/ijmqe/2017005](https://doi.org/10.1051/ijmqe/2017005)
- [22] Alberto Lavatelli, Emanuele Zappa, Uncertainty in vision based modal analysis: probabilistic studies and experimental validation, *Acta IMEKO* 5(4) (2016) pp.37-48.
DOI: [10.21014/acta_imeko.v5i4.426](https://doi.org/10.21014/acta_imeko.v5i4.426)

- [23] O. M. Vasilevskiy, Methods of determining the recalibration interval measurement tools based on the concept of uncertainty, *Technical Electrodynamics* 6 (2014) pp. 81-88.
DOI: [10.1051/ijmqe/2014017](https://doi.org/10.1051/ijmqe/2014017)
- [24] O. M. Vasilevskiy, P. I. Kulakov, I. A. Dudatiev, V. M. Didych, A. Kotyra, B. Suleimenov, A. Assembay, A. Kozbekova, Vibration diagnostic system for evaluation of state interconnected electrical motors mechanical parameters, *Proc. SPIE 10445, Photonics Applications in Astronomy, Communications, Industry, and High Energy Physics Experiments*, 104456C, 2017.
DOI: [10.1117/12.2280993](https://doi.org/10.1117/12.2280993)
- [25] S. Beckert, W. Paim, Critical analysis of the acceptance criteria used in measurement systems evaluation, *Int. J. of Metrol. Qual. Eng.* 8 (23) (2017) pp. 1-9.
DOI: [10.1051/ijmqe/2017016](https://doi.org/10.1051/ijmqe/2017016)
- [26] M. Beer, S. Ferson, V. Kreinovich, Imprecise probabilities in engineering analyses, *Mech. Syst. Signal Process* 37 (1-2) (2013) pp. 4-29.
DOI: [10.1016/j.ymssp.2013.01.024](https://doi.org/10.1016/j.ymssp.2013.01.024)
- [27] O. Vasilevskiy, P. Kulakov, D. Kompanets, O. Lysenko, V. Prysyzhnyuk, W. Wójcik, D. Baitussupov, A new approach to assessing the dynamic uncertainty of measuring devices, *Proc. SPIE 10808, Photonics Applications in Astronomy, Communications, Industry, and High-Energy Physics Experiments*, 108082E, 2018.
DOI: [10.1117/12.2501578](https://doi.org/10.1117/12.2501578)
- [28] R. Trishch, O. Nechuiviter, K. Dyadyura, O. Vasilevskiy, I. Tsykhanovska, M. Yakovlev, Qualimetric method of assessing risks of low quality products, *MM Science Journal* (2021) pp. 4769-4774.
DOI: [10.17973/MMSJ.2021_10_2021030](https://doi.org/10.17973/MMSJ.2021_10_2021030)
- [29] ISO, Guidelines for implementation of statistical process control (SPC) – part 1: elements of SPC, ISO 11462-1:2001 (2001).
- [30] J. Staniskisa, E. Katiluteb, Unsustainability reduction in enterprises by incremental innovations implementation and management, *Journal of Cleaner Production* 236 (2019) art. no. 117542.
DOI: [10.1016/j.jclepro.2019.07.017](https://doi.org/10.1016/j.jclepro.2019.07.017)
- [31] A. Chan, S. Ryan, J. Quarter, Supported social enterprise: a modified social welfare organization, *Non- Profit Vol. Sector Q.*, 46(2) (2017) pp. 261-279.
DOI: [10.1177/0899764016655620](https://doi.org/10.1177/0899764016655620)
- [32] ISO, Geometrical product specifications (GPS) – inspection by measurement of workpieces and measuring equipment – part 1: decision rules for proving conformity or nonconformity with specifications, ISO 14253-1:2013 (2013).
- [33] BIPM, IEC, IFCC, ISO, IUPAC, IUPAP, OIML, Evaluation of measurement data – the role of measurement uncertainty in conformity assessment, *Joint Committee for Guides in Metrology, JCGM 106:2012* (2012).