



# RESEARCH ON DISPERSION IN INDENTER AND REFERENCE BLOCK FOR ROCKWELL HARDNESS TEST

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## Abstract:

In this report, the Rockwell indenters and hardness reference blocks obtained from different three manufacturers were evaluated. And these results with the tolerances for the indirect verification prescribed in ISO 6508-2 and ASTM E18 were compared, it has been suggested that the tolerances prescribed in ASTM E18 might be too strict in view of actual circumstances.

**Keywords:** Rockwell indenter, hardness reference block, ISO/IEC 17025, ISO standards, ASTM standards

## 1. INTRODUCTION

The importance of ensuring the traceability in measurement has been increased in these years, and accordingly, the spread of systems certifying tests and calibrations in conformity with ISO/IEC 17025[1] that can publicly give assurance has been promoted in a worldwide manner. In addition, the Mutual Recognition Agreement (MRA) that mutually certifies the conformity assessment results of own country as equivalent to another country is implemented among many accredited systems, and the accredited certificates are valid in any countries. It can be said that this system is extremely beneficial for globalization of manufacturing and industry. The hardness test is no exception, and the number of cases where the calibration of hardness reference blocks, indenters and hardness testing machines is requested to conform to ISO/IEC 17025 is increasing. It can be said that the supply source of indenters and hardness reference blocks that are used for calibration of hardness testing machines does not matter if the testing and calibration are performed in conformity with accredited systems system. However, a hardness value is industrial quantity and has no physical reference, therefore, the traceability system and uncertainty evaluation method for measurement values and calibration values are not completely standardized in the global aspect under present circumstances. Such present circumstances may become a problem for

calibration of hardness testing machines. We know that even differences in hardness values among national metrology institute level are a problem for calibration of actual hardness testing machines [2]. In this report, evaluating the dispersion of Rockwell indenters and hardness reference blocks obtained from different three manufacturers have been conducted for the purpose of investigating the realistic circumstances. Then, based on these results, the uncertainty of calibration in indirect verification of the hardness testing machine was estimated, and the consistency with the tolerance value prescribed in the standard was investigated.

## 2. EXPERIMENT

Three pieces of Rockwell diamond conical indenters, tungsten carbide ball indenters with 1.5875 mm in diameter and six types of hardness reference blocks from three manufacturers are obtained. The scales and hardness levels of the six hardness reference blocks were 30 HRC, 60 HRC, 90 HR15N, 30 HRBW, 90 HRBW and 35 HR15TW. Three manufacturers are hereinafter referred to as Manufacturer A, Manufacturer B, and Manufacturer C. Manufacturer A is a famous indenter and reference block manufacturer in Europe. Manufacturer B and Manufacturer C are US manufacturers and a lot of their products are widespread in the United States. An accredited certificate is issued for all of these indenters and reference blocks to prove that calibration of them conforming to ISO/IEC 17025 has been conducted. SHT-31, a Rockwell hardness standard testing machine manufactured by Mitutoyo Corporation, was used for evaluation. The specifications and accuracy of each part of the testing machine is conformed to ISO 6508-3: calibration of the hardness reference block [3]. Moreover, the testing conditions such as time of loading the testing force and duration time were set according to this standard.

## 2.1. Results of evaluating indenters of each manufacturer

Testing on the same reference block with the use of obtained indenters and our indenter were conducted. Our indenter, i.e. Mitutoyo indenter is conformable to ISO 6508-3, and is equivalent to an indenter classified in Class A prescribed in ASTM E18[4]. The differences between the hardness values of the targeted indenters to be evaluated and the hardness value of our indenter were evaluated. Figure 1 shows the differences of hardness values in each scale. The medians were regarded as the average of the differences of hardness values in each scale. The value  $P_1$  shows a 95% confidence interval of dispersion calculated by multiplying the experimental standard deviation of the differences of hardness values in each scale by a coverage factor. Here, the coverage factor was determined to be 2.31 on the basis of the Student's t-distribution in consideration that the degree of freedom of data in each scale is 8.

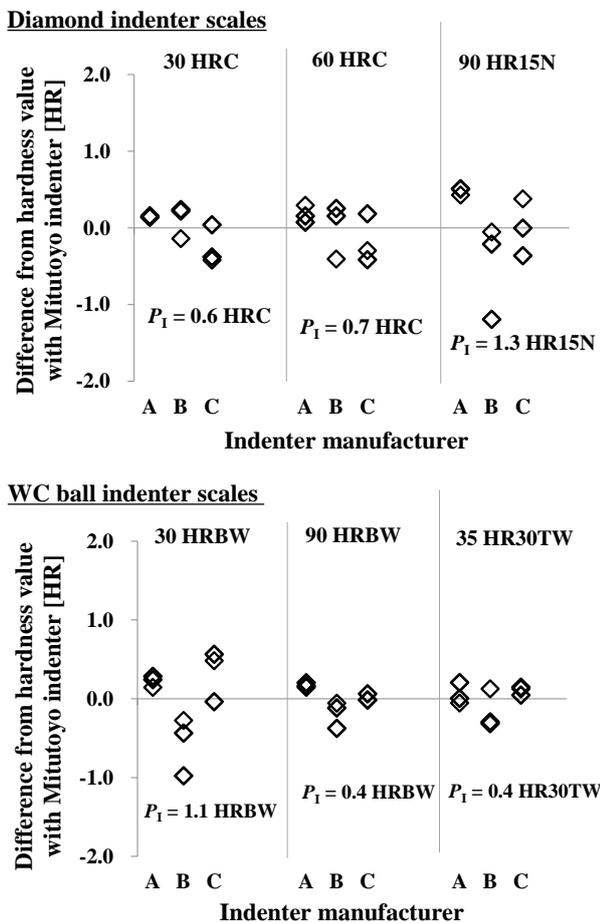


Figure 1: Difference from hardness value with Mitutoyo indenter

## 2.2. Results of evaluating obtained reference blocks of each manufacturer

Testing on the obtained reference blocks with the use Mitutoyo indenter were conducted, and the

measured hardness values were compared with the calibration values of the targeted hardness reference blocks to be evaluated. Figure 2 shows the differences from the calibration values of the reference blocks in each scale. The medians were regarded as the average of the differences of hardness values in each scale. The value  $P_B$  shows a 95% confidence interval of dispersion calculated by multiplying the experimental standard deviation of the differences of hardness values in each scale by a coverage factor. Here, the coverage factor was determined to be 2.31 on the basis of the Student's t-distribution in consideration that the degree of freedom of data in each scale is 8.

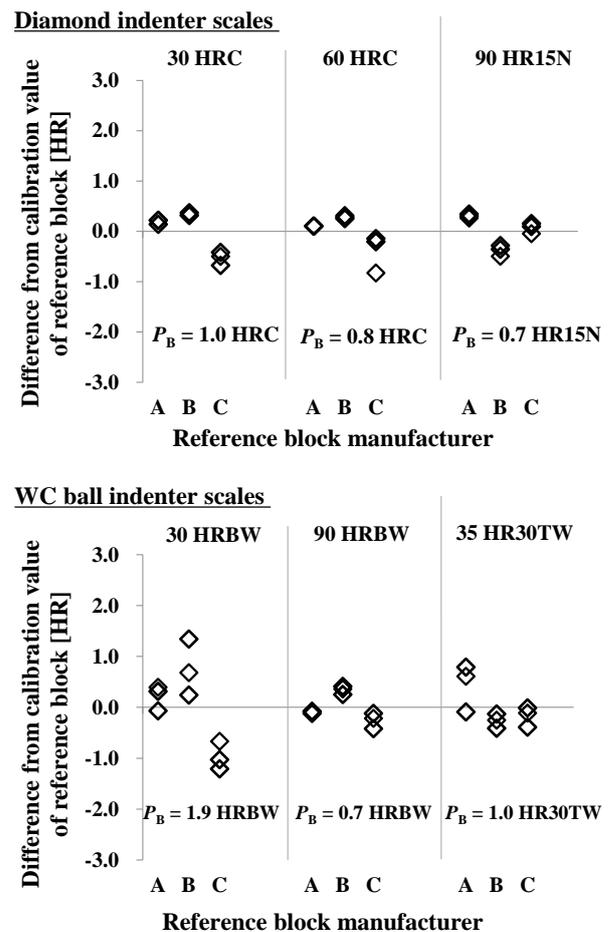


Figure 2: Differences from the calibration values of the reference blocks

## 3. DISCUSSION

### 3.1. Regarding results of evaluating indenters

Table 1 shows the  $P_1$  value in Fig. 1 and the tolerance of indenter prescribed in ISO 6508-2[5] and ASTM E18. For diamond indenter, the difference from the reference indenter is prescribed in standard as tolerance. There are some  $P_1$  values that are larger than the tolerance. This fact suggests that indenters whose tolerance exceeds the standards may be on the market.

For tungsten carbide ball indenter, the difference from the calibration value of reference block is in standard as tolerance. Except for 30 HRBW, the  $P_1$  value is sufficiently smaller than the tolerance of standard. However, this result is a difference from the value measured with the same testing machine and test conditions, and the uncertainty of the calibration value of reference block is considered to be larger than measured value. That is, the fact that the  $P_1$  value is smaller is expected result. Nevertheless, for 30 HRBW, the  $P_1$  value exceeds the tolerance of ASTM standard. In addition, there is a bias of indenters among manufacturers. That is, for 30 HRBW, it is suggested that the use of indenter from another manufacturer may exceed the tolerance of ASTM standard.

Table 1: Evaluation results of indenter and tolerance of standard

Scale	Tolerance (ISO 6508-2)	Tolerance (ASTM E18)	Experimental result ( $P_1$ value)
30 HRC	0.8 HRC	0.8 HRC	0.6 HRC
60 HRC	0.8 HRC	0.4 HRC	0.7 HRC
90 HR15N	0.8 HR15N	0.5 HR15N	1.3 HR15N
30 HRBW	4.0 HRBW	0.8 HRBW	1.1 HRBW
90 HRBW	2.0 HRBW	0.8 HRBW	0.4 HRBW
35 HR30TW	3.0 HR30TW	0.8 HR30TW	0.4 HR30TW

### 3.2. Estimation of uncertainty for indirect verification using results of evaluating reference block.

The disperse i.e. uncertainty of hardness values generated in the indirect verification of the testing machine was estimated. As factors for the uncertainty, we hypothesized the influences of the depth measuring device, difference of the indenter with respect to the reference indenter, the calibration value and uniformity of the hardness reference block, and machine hysteresis. It thought that the testing force, indentation time, and duration time of testing force can be ignored because these factors have little influence. The standard uncertainty for each factor was estimated based on the description in Table 2. If a tolerance is different between the ISO standards and ASTM standards, stricter tolerance was used for estimation. Table 3 shows the uncertainty budget for each scale.

Table 2: Hypothesized uncertainty factors

Uncertainty factors	Hypothesized variation of hardness values
Depth measuring device	Tolerances in verification of depth measuring device prescribed in ISO 6508-2 and ASTM E18
Diamond indenter	Tolerance of difference in hardness value from reference indenter at testing with the identical reference block prescribed in ASTM E18
Ball indenter	Tolerance of difference in calibration value from reference block at testing reference block prescribed in ASTM E18
Uniformity of reference block	Tolerance of difference between the maximum and minimum values in 5-point measurement prescribed in standard for reference block, ISO 6508-3 or ASTM E18
Calibration value of reference block	$P_B$ values in Fig. 2 are hypothesized as expanded uncertainty.
Machine deformation	Although the tolerance is $\pm 1.0$ HR in ISO 6508-2 or ASTM E18, it is hypothesized to be $\pm 0.3$ HR in view of actual circumstances.

### 3.3. Regarding consistency with the tolerance of the standard

Table 4 shows the tolerances in indirect verification prescribed in ISO 6508-2, ASTM E18 and estimated expanded uncertainty. When the expanded uncertainty of the hardness value in indirect verification is compared with the tolerance of the standard, it is considered that the uncertainty is within the tolerance range of the ISO standards in all the evaluated scales. With regard to the ASTM standards, on the other hand, the uncertainty may not be within the tolerance range except for 30 HRBW and 35 HR30TW through the indirect verification even with the use of indenters and reference blocks that are conformable with the standards. The tolerance of 30 HRBW in the ASTM standards was revised from  $\pm 1.5$  HRBW to  $\pm 2.5$  HRBW in 2019, and it is thought that review in light of present circumstances is conducted. However, even for 30 HRBW and 35 HR30TW, the margin for the tolerance is small, and the tolerance may not be appropriate.

In this report, the estimated expanded uncertainty of the hardness value in indirect verification is the result of extracting only main uncertainty factors, and is obtained by using the smaller tolerance between two types of standards. In addition, experimental estimation of indenters and hardness reference blocks was conducted only about three manufacturers. Thus, the actual uncertainty may be even larger. Regardless of the above, when the dispersion is compared with the tolerance of the ASTM standards, the dispersion is equivalent to or

exceeds the tolerance. Especially regarding 60 HRC, the difference between the tolerance  $\pm 0.5$  HRC of indirect verification prescribed in the ASTM standards and the dispersion of the estimated hardness values is large. This fact suggests that the tolerance of ASTM standards is not realistic.

Table 3: Uncertainty budget for each scale

30 HRC				
Factor	Range ( $\pm$ )	Distribution	Divisor	Standard uncertainty
Depth measuring	0.5 HRC	Rectanglar	$\sqrt{3}$	0.289 HRC
Indenter	0.4 HRC	Rectanglar	$\sqrt{3}$	0.231 HRC
Uniformity of block	0.35 HRC	Rectanglar	$\sqrt{3 \times \sqrt{5}}$	0.090 HRC
Uncertainty of block	1.0 HRC	Normal	2	0.500 HRC
Machine hysteresis	0.3 HRC	Rectanglar	$\sqrt{3}$	0.173 HRC
Combined standard uncertainty				0.652 HRC
Expanded uncertainty ( $k = 2$ )				1.3 HRC

60 HRC				
Factor	Range ( $\pm$ )	Distribution	Divisor	Standard uncertainty
Depth measuring	0.5 HRC	Rectanglar	$\sqrt{3}$	0.289 HRC
Indenter	0.4 HRC	Rectanglar	$\sqrt{3}$	0.231 HRC
Uniformity of block	0.2 HRC	Rectanglar	$\sqrt{3 \times \sqrt{5}}$	0.052 HRC
Uncertainty of block	0.8 HRC	Normal	2	0.400 HRC
Machine hysteresis	0.3 HRC	Rectanglar	$\sqrt{3}$	0.173 HRC
Combined standard uncertainty				0.574 HRC
Expanded uncertainty ( $k = 2$ )				1.1 HRC

90 HR15N				
Factor	Range ( $\pm$ )	Distribution	Divisor	Standard uncertainty
Depth measuring	0.5 HR15N	Rectanglar	$\sqrt{3}$	0.289 HR15N
Indenter	0.5 HR15N	Rectanglar	$\sqrt{3}$	0.289 HR15N
Uniformity of block	0.25 HR15N	Rectanglar	$\sqrt{3 \times \sqrt{5}}$	0.065 HR15N
Uncertainty of block	0.7 HR15N	Normal	2	0.350 HR15N
Machine hysteresis	0.3 HR15N	Rectanglar	$\sqrt{3}$	0.173 HR15N
Combined standard uncertainty				0.569 HR15N
Expanded uncertainty ( $k = 2$ )				1.1 HR15N

30 HRBW				
Factor	Range ( $\pm$ )	Distribution	Divisor	Standard uncertainty
Depth measuring	0.5 HRBW	Rectanglar	$\sqrt{3}$	0.289 HRBW
Indenter	0.8 HRBW	Rectanglar	$\sqrt{3}$	0.462 HRBW
Uniformity of block	0.5 HRBW	Rectanglar	$\sqrt{3 \times \sqrt{5}}$	0.129 HRBW
Uncertainty of block	1.9 HRBW	Normal	2	0.950 HRBW
Machine hysteresis	0.3 HRBW	Rectanglar	$\sqrt{3}$	0.173 HRBW
Combined standard uncertainty				1.116 HRBW
Expanded uncertainty ( $k = 2$ )				2.2 HRBW

90 HRBW				
Factor	Range ( $\pm$ )	Distribution	Divisor	Standard uncertainty
Depth measuring	0.5 HRBW	Rectanglar	$\sqrt{3}$	0.289 HRBW
Indenter	0.8 HRBW	Rectanglar	$\sqrt{3}$	0.462 HRBW
Uniformity of block	0.35 HRBW	Rectanglar	$\sqrt{3 \times \sqrt{5}}$	0.090 HRBW
Uncertainty of block	0.7 HRBW	Normal	2	0.350 HRBW
Machine hysteresis	0.3 HRBW	Rectanglar	$\sqrt{3}$	0.173 HRBW
Combined standard uncertainty				0.676 HRBW
Expanded uncertainty ( $k = 2$ )				1.4 HRBW

35 HR30TW				
Factor	Range ( $\pm$ )	Distribution	Divisor	Standard uncertainty
Depth measuring	0.5 HR30T <sup>a</sup>	Rectanglar	$\sqrt{3}$	0.289 HR30TW
Indenter	0.8 HR30T <sup>a</sup>	Rectanglar	$\sqrt{3}$	0.462 HR30TW
Uniformity of block	0.5 HR30T <sup>a</sup>	Rectanglar	$\sqrt{3 \times \sqrt{5}}$	0.129 HR30TW
Uncertainty of block	1.0 HRBW	Normal	2	0.500 HR30TW
Machine hysteresis	0.3 HR30T <sup>a</sup>	Rectanglar	$\sqrt{3}$	0.173 HR30TW
Combined standard uncertainty				0.770 HR30TW
Expanded uncertainty ( $k = 2$ )				1.5 HR30TW

Table 4: Tolerance of standards and estimated extended uncertainty in indirect verification

Scale	Tolerance (ISO 6508-2)	Tolerance (ASTM E18)	Analysis (Expanded uncertainty)
30 HRC	1.5 HRC	1.0 HRC	1.3 HRC
60 HRC	1.5 HRC	0.5 HRC	1.1 HRC
90 HR15N	2.0 HR15N	0.7 HR15N	1.1 HR15N
30 HRBW	4.0 HRBW	2.5 HRBW	2.2 HRBW
90 HRBW	2.0 HRBW	1.0 HRBW	1.4 HRBW
35 HR30TW	3.0 HR30TW	1.5 HR30TW	1.5 HR30TW

#### 4. SUMMARY

The following items including verification and evaluation were conducted and described in this report.

- Evaluation of the dispersion of indenters and hardness reference blocks which are in the market.
- Comparison of evaluation result and tolerances for indenter.
- Estimation of uncertainty of hardness value in indirect verification of the testing machine based on the evaluation result of the reference block.
- Verification of validity of the tolerance in the indirect verification prescribed in the ISO standards and ASTM standards.

By conducting the items above, and the following were found.

- For diamond indenter, there is a possibility that the indenters exceed the tolerance of standard are in market.
- For tungsten carbide ball indenters, there is a possibility that the difference may exceed the tolerance of standard for 30 HRBW if the indenter manufacturer changes.
- It was suggested that the estimated dispersion of the hardness values generated in indirect verification fell under the tolerance range of the ISO standards.
- It was suggested that the estimated dispersion of the hardness values generated in indirect verification exceed the tolerance range of the ASTM standards, and in particular, the tolerance of ASTM standard for 60 HRC may be too strict.

#### 5. CONCLUSION

A hardness value is not a physical quantity, but an industrial quantity obtained by a prescribed testing method. The fact is that testing machines and testing conditions vary within the prescribed tolerance range and relatively large dispersion of hardness values is observed even in a national standard level. If the fact that this is a destructive

test in which absolute reference does not exist is considered, it can be said that such dispersion is generated as a matter of course. On the other hand, under such circumstances, accredited systems and traceability are utilized. This type of issue may be a big problem that cannot be solved by company alone for manufacturers of hardness testing machines in each country. We hope that verification of consistency with public standards becomes emphasis for the sake of the industrial world.

## 6. REFERENCES

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