

Techno-economics of “Teal” Hydrogen Production via Combined Steam Methane Reforming and Biomass Gasification

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The global transition towards net-zero greenhouse gas emissions establishes a need for cleaner energy technologies. Hydrogen is a promising energy carrier whose global demand is steadily increasing and is conventionally produced through steam-methane reforming with carbon capture, or blue H₂. Hydrogen production supplied by renewable energy (green H₂) is an emerging process, but developing countries are not yet ready for a full transition. Augmenting blue H₂ with green H₂ production will allow a smoother transition until green H₂ costs significantly decrease by 2050. In this work, a novel, low-cost teal hydrogen (teal H₂) plant, a mixture of blue and green H₂ technologies, located in the Philippines which combines steam-methane reforming, rice husk gasification, and carbon capture by monoethanolamine absorption, is proposed. Setting a production rate of 9,000 kg H₂/h, the techno-economic potential of five cases with varying natural gas to rice husk contribution ratios were evaluated using AspenPlus. The levelized cost of the 25:75 teal H₂ case at 1.06 USD/kg is cheaper than blue H₂ and green H₂ by 4.37 and 2.34 USD/kg, respectively. Moreover, the CO₂-equivalent emissions of the 25:75 teal H₂ case at 0.002 t CO₂-eq/1,000 Nm³ H₂ is 57.10 % and 39.25 % lower than those from blue H₂ and green H₂. As green H₂ becomes more economical, rice husk feed to the gasification process can be gradually increased to favor biomass- over petroleum-derived H₂. This case study is a successful proof of concept that teal H₂ may help transition the energy sector to carbon neutrality.

1. Introduction

The Paris Agreement is a global mandate that legally binds countries to reduce greenhouse gas emissions and achieve a climate neutral world by the mid-21st century, driving the development of renewable and green technology and industrial processes (United Nations, 2015). Hydrogen is a clean-energy carrier that has the potential to reduce reliance on coal- and gas-generated electricity. Its demand in the chemical industry is expected to increase by 31 % by 2030 (International Energy Agency, 2019). Hydrogen is conventionally produced from the reforming of natural gas (i.e., steam-methane reforming, SMR) or gasification of coal. To reduce emissions, two production pathways are at the center of research trends: (i) blue hydrogen and (ii) green hydrogen production. Blue hydrogen is produced when conventional hydrogen plants are simply augmented with carbon capture technologies to store and utilize the carbon dioxide by-product. On the other hand, green hydrogen relies on water electrolysis, biomass gasification (BG), and renewable technologies (Noussan et al., 2020).

With around 98 % of current hydrogen production derived from fossil-fuels, blue H₂ is the more accessible technology with hundreds of commercial and pilot plants across the globe (Global CCS Institute, n.d.). Blue H₂ is the more mature production pathway with costs ranging from 1.40 to 2.40 USD/kg, which is lower than the cost of green H₂ at 2.30 to 7.70 USD/kg. However, green H₂ is capable of becoming a carbon-neutral or carbon-negative pathway, provided that it is powered by renewable energy (Ibrahim et al., 2021).

Developing countries have difficulties in a full transition to either H₂ production pathway, because they lack the infrastructure for commercial blue H₂ and emerging green H₂ technologies. However, international and intergovernmental reports project an 80 % reduction in green H₂ costs by 2050; whereas blue H₂ costs are forecasted to stagnate (Newborough and Cooley, 2020). In addition, increasing reliance on renewable feedstock is expected due to concerns such as decreasing fossil fuel supply, price uncertainty, and environmental effects (Peres et al., 2013). In line with the ongoing global discussion, blue H₂ is seen as a short-term solution to reduce emissions, while green H₂ is regarded as the long-term solution to cleaner hydrogen production once its techno-economic challenges have been addressed (Newborough and Cooley, 2020). As such, this paper proposes a novel “teal” hydrogen plant, which augments the conventional steam-methane reforming plus carbon capture (SMR+CC, blue H₂) process with biomass gasification (BG, green H₂). Its techno-economic potential is assessed through process simulations with varying feed ratios for blue and green H₂ production and evaluations of the levelized cost of hydrogen (LCOH) for each scenario. The proposed teal H₂ plant may serve as a guide for developing countries to start investing in existing commercial hydrogen production and transitioning to greener technologies as costs drop in the long term.

2. Methodology

The methodology is divided into five parts. First, the modeling scenarios and plant location were introduced. Second, an overview of the hydrogen production process was discussed. Third, the techno-economic values and assumptions were shown. Fourth, the different scenarios were simulated in Aspen Plus (2017) and presented. Lastly, the profitability metrics to assess the H₂ plants were presented.

2.1 Case studies

Setting the production capacity to 9,000 kg H₂/h, five case studies were compared to determine the sensitivity of the LCOH to changes in feed. Three cases of the teal H₂ plant were considered with varying natural gas (NG) and rice husk (RH) feed flow rates, adjusted based on their set contributions to the H₂ production capacity. The breakdown of the three variations are as follows: 1) 25 % of H₂ produced is made from NG & 75 % made from RH; 2) 50 % NG & 50 % RH; and, 3) 75 % NG & 25 % RH. Two other cases, namely the blue H₂ plant (SMR + CC; 100 % NG) and green H₂ plant (BG + CC; 100 % RH), were considered for comparison.

The chosen plant location is in Batangas, Philippines given its proximity to liquefied NG import terminals targeted to be in place by 2022-2025 (Reynolds, 2021) and the opportunities for CO₂ storage in Malampaya, Palawan with the anticipated shutdown of the Malampaya Gas Fields (Asian Development Bank, 2013).

2.2 Process description

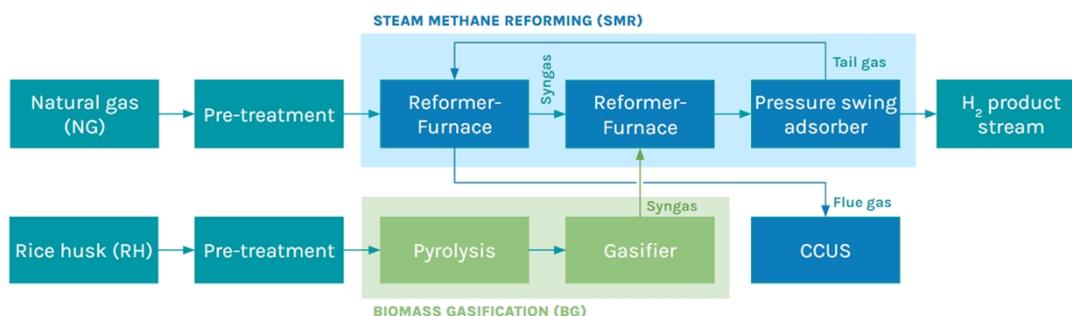


Figure 1: Block-flow diagram of proposed novel teal hydrogen production plant

The process, simulated using AspenONE Suite (Aspen Plus (2017), Aspen Adsorption (2017), & Aspen Energy Analyzer (2017)), can be divided into three units: the steam methane reforming unit (blue H₂), the biomass gasification unit (green H₂), and the carbon capture (CC) unit, as shown in Figure 1. The reactions involved in the main process units (SMR and BG) are summarized in Table 1.

In the Steam Methane Reforming unit, the fed natural gas is split into two streams: (1) feedstock for the reformer process, and (2) supplementary fuel for the steam reformer furnace. The feedstock NG undergoes 6 units: desulfurization (Eq(1) & Eq(2)), sulfur adsorption (Eq(3)), pre-reformer (Eq(4), Eq(5), Eq(6)), main reformer (Eq(7) & Eq(8)), water-gas shift (WGS) reactor (Eq(9)), and pressure swing adsorber (PSA). Streams before the pre-reformer and the main reformer are mixed with an excess amount of steam to achieve a steam-to-carbon ratio of 3.0 and 5.0, respectively. The heat of the reaction in the main reformer is supplied by the furnace where the combustion of fuel natural gas and air occurs. The flue gas resulting from the combustion proceeds to the carbon capture unit. Meanwhile, syngas from BG is mixed with the reformer syngas before entering the WGS

reactor. Afterward, the PSA tail gas is recycled back to the furnace as fuel for combustion. The high-purity hydrogen stream is further compressed based on the product requirements.

Furthermore, the overall process of biomass gasification can be modelled in three stages, which include drying (Eq(10)), pyrolysis, and gasification (Eq(11)). It is hypothesized that any phase transition in the gasification process is stable and, thus, the equilibrium model may be based on the Gibbs free energy minimization principle. Some other important assumptions include: (i) O, H, N, and S are in the gaseous phase while C undergoes incomplete transformation to gas, (ii) rice husk ash is inert, (iii) the gasifier remains stable and parameters are time-independent, (iv) all gas-phase reactions in the biomass gasifier are instantaneous and will reach equilibrium, (v) biomass particles are at a uniform temperature, and (vi) the reactions are isobaric (Vassilev et al., 2010). The syngas produced is then mixed with that from SMR and sent to the water-gas shift reactor. After cooling to 40 °C, the reformer flue gas is sent to the bottom stage of the absorber column where lean MEA (30 wt%, 0.25 mol CO₂/mol MEA) absorbs CO₂ by reactive distillation. The decarbonized flue gas is then washed with water to remove excess MEA before it is sent to the stack to be released into the air. The now rich MEA solvent is regenerated by a stripper (114 °C, 1.8 bar) with a partial condenser and partial reboiler. The captured CO₂ in the stripper is then compressed for storage. The condensate of the partial condenser is recycled to the absorber's water-wash section, whose bottoms stream is mixed with MEA makeup. A purge stream is added to prevent the accumulation of H₂O.

From these simulations, the required feed (NG, RH, and MEA), H₂ product flow rate and purity, and CO₂-eq emissions are obtained for the five cases.

Table 1: Summary of reactions in the SMR and BG facilities of the proposed Teal H₂ plant

| Reaction | Eq | Operating Conditions | Ref. |
|---|------|------------------------------|------|
| Desulfurization Unit: Hydrogenolysis and H ₂ S Removal | | | |
| C ₄ H ₈ S (tetrahydrothiophene) + 2H ₂ → n-C ₄ H ₁₀ + H ₂ S | (1) | 380.2 °C, 36.28 bar | [a] |
| C ₄ H ₄ S (thiophene) + 4H ₂ → n-C ₄ H ₁₀ + H ₂ S | (2) | | |
| ZnO + H ₂ S → ZnS + H ₂ O | (3) | | |
| Pre-Reformer | | | |
| C _n H _m + nH ₂ O → nCO + (n + ½m)H ₂ | (4) | 450 °C, 24 bar | [a] |
| CO + 3H ₂ ↔ CH ₄ + H ₂ O | (5) | | |
| CO + H ₂ O ↔ CO ₂ + H ₂ | (6) | | |
| Main Reformer | | | |
| CH ₄ + H ₂ O ↔ 3H ₂ + CO | (7) | 450 °C, 24 bar | [b] |
| CH ₄ + 2H ₂ O ↔ 4H ₂ + CO ₂ | (8) | | |
| Water Gas Shift Reactor | | | |
| CO + H ₂ O → CO ₂ + H ₂ | (9) | 313 °C, 28 bar | [a] |
| Biomass Gasification | | | |
| Rice husk → 0.0556 H ₂ O | (10) | 610 °C, 1 bar (Pyrolysis) | [c] |
| Dry rice husk → ash + gases (e.g., CO, CH ₄ , CO ₂ , H ₂ , H ₂ O) + carbon | (11) | 850 °C, 1 bar (Gasification) | |

[a] (Twigg, 2018), [b] (Sharma et al., 2019), [c] (Liu et al., 2016)

2.3 Techno-economic data

The feasibility of the teal H₂ plant was assessed by investment analysis. Fixed capital investments (FCI), operating costs, and other important assumptions are listed in Table 2 for a total plant life of N = 27 years, which includes 2 years in construction, and a 24-h operation with 30 days downtime per year. The plant was assumed to be funded at 40 % equity with the balance coming from a 6 % interest rate bank loan. During operation, the sales were simulated to gradually increase from a 50 % turnover to a 100 % turnover by the 16th year of operation.

Table 2: Techno-economic modelling parameters to determine the LCOH of cases 1 to 5.

| Production ratio (Blue H ₂ :Green H ₂) | Case 1 (100:0) | Case 2 (75:25) | Case 3 (50:50) | Case 4 (25:75) | Case 5 (0:100) | Ref |
|--|-------------------|-------------------|-------------------|-------------------|-------------------|------|
| Capital costs (mil USD) | 287.820 | 495.673 | 791.013 | 1,070.098 | 1,137.899 | [a], |
| Operating costs (mil USD/y) | 643.476 | 542.850 | 454.105 | 365.037 | 490.131 | [b] |
| Plant capacity (MW) | 174.075 | 290.060 | 290.027 | 304.967 | 258.036 | |

[a] (Wittholz et al., 2008), [b] (Sinnott and Towler, 2020). Other costs adapted from Aspen Plus (2017) and Aspen Energy Analyzer (2017). Operating costs at 100 % plant loading.

2.4 Scenario modeling

The simulation for the whole teal H₂ plant is shown in Figure 2, which represents the five cases. For case 1 (blue H₂), the biomass gasification facility of the plant is deactivated. For case 5 (green H₂), the steam-methane reforming facility is deactivated, syngas from gasification is redirected to the low- and high-temperature water-gas shift reactor, and PSA tail gas is directed to the CC unit.

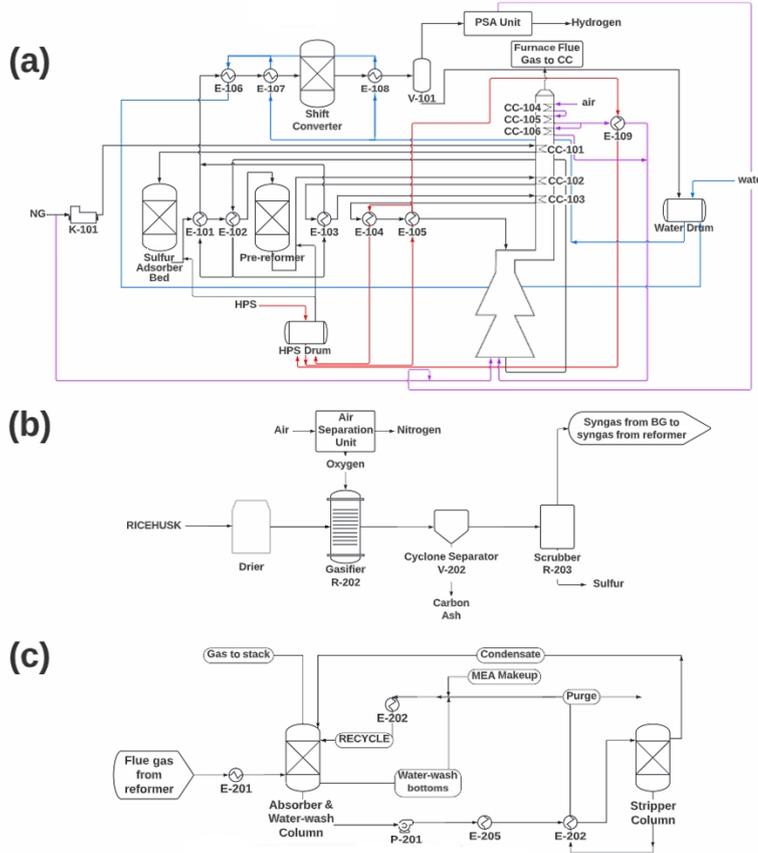


Figure 2: Process flow diagrams of the proposed teal H₂ plant, (a) steam-methane reforming facility and its utilities, (b) biomass gasification, and (c) carbon capture. The blue lines represent the cold utility stream, the red lines represent the hot utility stream, and the purple lines represent the furnace feed

2.5 Techno-econometric metrics

The techno-economic potential of the five cases in the teal H₂ simulation were assessed based on the following parameters: CO₂ capture rate, net present value (NPV), payback period (PBP), internal return rate (IRR), and LCOH. The last four parameters were obtained using the built-in spreadsheet functions. Note that the LCOH was calculated by finding the IRR that would result to a zero NPV, at which point the selling price of hydrogen equates to its production cost. Furthermore, plant revenue included sales projection of the produced H₂ and captured CO₂ based on market prices.

3. Results and discussion

The techno-economic metrics of the optimized simulations are presented below to assess whether teal H₂ is a feasible and profitable alternative to blue H₂ production (case 1).

3.1 Techno-economic metrics

The results of the techno-economic analysis for each case are presented in Table 3. With each case, the NG feed decreases as more RH feed was introduced to attain a constant production rate of 9,000 kg H₂/h. It has been found that the decrease in NG feed is not proportional to the increase of RH from one case to the other. This demonstrates that given equal amounts of feed, SMR can produce more H₂ than BG. However, the cheaper price of RH makes BG more attractive. Therefore, intermediate cases that combine SMR and BG were simulated to reduce total feed costs while maintaining high conversion.

Table 3: Techno-economic metrics describing each simulation

| | Case 1 (100:0) | Case 2 (75:25) | Case 3 (50:50) | Case 4 (25:75) | Case 5 (0:100) |
|---|----------------|----------------|----------------|----------------|----------------|
| NG feed (kg/h) | 29,951.00 | 22,463.25 | 14,977.00 | 7,487.75 | - |
| RH feed (kg/h) | - | 13,470.00 | 45,795.00 | 86,600.00 | 99,700.00 |
| CO ₂ captured (kg/h) | 80,237.44 | 70,545.16 | 88,813.50 | 103,797.80 | 98,633.23 |
| Carbon capture rate (%) | 97.78 | 97.59 | 97.96 | 98.34 | 97.47 |
| CO ₂ -eq emissions (t/1,000 Nm ³ H ₂) | 0.004765358 | 0.003062251 | 0.002461588 | 0.002044461 | 0.003365320 |
| LCOH (USD/kg) | 5.43 | 4.83 | 2.86 | 1.06 | 3.40 |

Case 1 exhibits the highest LCOH value. This is higher than the LCOH values of SMR processes found in literature (Global CCS Institute, 2021), which stems from higher NG import price and lower amount of CO₂ captured. As the NG feed share decreases across cases, LCOH also decreases, with case 4 exhibiting the lowest value. This trend can be attributed to two factors: first, the decrease of high-cost NG combined with the increased share of low-cost RH to H₂ production; and second, the increase in CO₂ captured contributing to a rise in revenue. The abrupt increase seen in Case 5 can be attributed to the higher capital and operating costs required, especially when compared to cases 3 and 4, given that full reliance on green H₂ costs significantly more at present. Moreover, the CO₂-eq emissions exhibit the same trend as that of LCOH values, with the CO₂-eq emissions of case 4 being 57.10 % and 39.25 % lower than that of case 1 and 5, respectively. Notably, the PSA tail gas of case 5 is methane-rich, which could both be a source of fuel gas because of its higher heating value and an additional hydrogen source (Thomson et al., 2020). Therefore, a reformer-furnace was added to utilize this stream.

3.2 Profitability and sensitivity analysis

The NPV, PBP, and IRR of the five cases for varying H₂ selling prices (USD/kg) are shown in Figure 3. When priced between 2 to 6 USD/kg, Case 4 is profitable since it exhibited positive NPV, PBP as low as 6.9 years, and an IRR as high as 22.6 %. Considering current average market prices for blue H₂ at 2 USD/kg and green H₂ at 5 USD/kg (Global CCS Institute, 2021), cases 3 and 4 present competitive pricing and high returns.

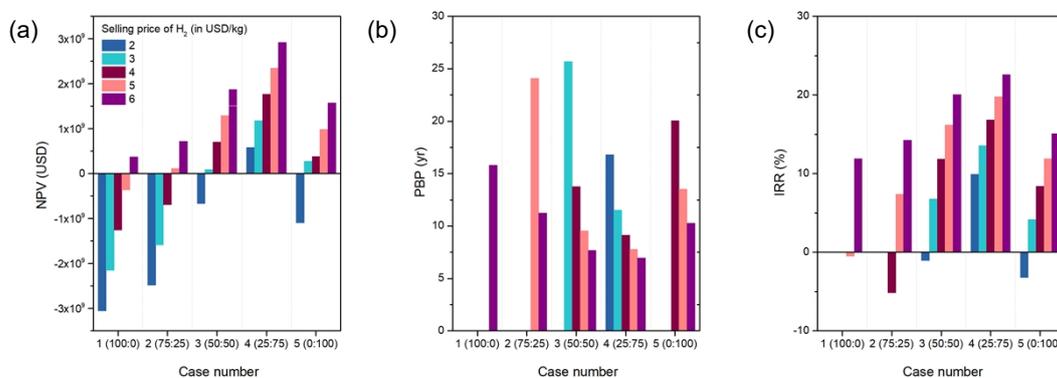


Figure 3: NPV (a), PBP (b), and IRR (c) of the five cases of hydrogen production (blue H₂:green H₂) at selling prices from 2 to 6 USD/kg H₂. Absence of PBP means 'no payback' and absence of IRR denotes a negative return rate

4. Conclusions

In this work, techno-economic case studies and profitability analyses were conducted on five cases of hydrogen production plants to determine if the proposed teal H₂ plant is suitable and practical, specifically for developing countries. The techno-economic metrics suggest that a 25:75 teal H₂ plant has the lowest LCOH of 1.06 USD/kg H₂ and emissions of 0.002 t CO₂-eq/1,000 Nm³ H₂ for a capacity of 9,000 kg/H₂, when compared to a fully blue or green H₂ plant. Moreover, the profitability analysis also suggests that a 25:75 teal H₂ plant is profitable at prices comparable to current blue and green H₂ prices. Its sound economic parameters (IRR, PBP, NPV) indicate that teal H₂ is an attractive investment for companies and governments as it considers available commercial infrastructures and future trends in hydrogen demand and prices.

This study serves as proof of concept that teal H₂ is future-fit, market competitive, and economically feasible as a transition into green hydrogen technologies. This is also a call to sustain research and development in green production and to achieve global environmental commitments. Future work will involve simulating other NG to biomass ratios not considered in this study, adding range of values around the input parameters (e.g., raw material, utility, and product prices), testing the synergies of other forms of blue (chemical-looping combustion, auto-thermal reforming, etc.) and green (electrolyzers) H₂ production, and pilot testing of the proposed teal H₂ plant.

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