

BIHARMONIC REPRESENTATION OF THE SOLUTION TO EQUILIBRIUM PROBLEM OF A PLATE MADE OF A COSSERAT MATERIAL

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The paper deals with a generalized plane stress problem in a Cosserat plate. There are given representations of the displacement and infinitesimal rotation fields that reduce the equilibrium problem to a single biharmonic equation involving a deflection function.

1. Introduction

In the previous paper [1] Author has reported a biharmonic representation of the displacement vector concerning a generalized plane state of stress (GPSS) in an elastic layer made of a Grioli-Toupin material. Such a representation of the displacement vector reduces the problem of bending of an elastic layer to one biharmonic equation

$$\nabla^4 v(x^\alpha) = 0 \quad (1.1)$$

Here $v(x^\alpha)$ stands for the layer deflection.

Similar representations for the displacement vector and vector of an infinitesimal rotation in the case of GPSS of a Cosserat medium have not been reported in the hitherto existing literature. In the present paper a generalization of the solution given in by the Author [1] to the Cosserat medium case will be put forward.

The summation convention is adopted. The Latin indices run over 1,2,3 and Greek ones – over 1,2. Comma implies partial differentiation.

2. Fundamental equations of the Cosserat medium

Following the notation of Nowacki [2,3] and Palmov [4] one can write down the constitutive relationships of an isotropic homogeneous and centrosymmetric

medium in the form

$$\sigma_{ij} = (\mu + \alpha)\gamma_{ij} + (\mu - \alpha)\gamma_{ji} + \lambda\gamma^k{}_k\delta_{ij} \quad (2.1)$$

$$\mu_{ij} = (\gamma + \varepsilon)K_{ij} + (\gamma - \varepsilon)K_{ji} + \beta K^k{}_k\delta_{ij}$$

The stress tensor is denoted by (σ_{ij}) and the couple-stress tensor by (μ_{ij}) ; (δ_{ij}) is Kronecker delta; (γ_{ij}) and (K_{ij}) are components of the deformation tensors. They are defined by

$$\gamma_{ij} = u_{j,i} - \epsilon^k{}_{ij}\phi_k \quad K_{ij} = \phi_{j,i} \quad (2.2)$$

(ϵ_{ijk}) represents the Levi-Civita permutation symbol; (u_i) are components of the displacement vector; (ϕ_i) represents components of the vector of infinitesimal rotations. Symbols μ , λ , α , γ , ε and β stand for the material constants of the Cosserat medium. The constants μ and λ can be viewed as Lamé moduli. Relations between the Nowacki-Palmov constants and the constants used by other authors are set up in Table 1.

Table 1

Authors	Material constants					
Nowacki [2] Palmov [4]	μ	λ	α	γ	ε	β
Aéro [5] Kuvshinskiĭ	μ	λ	$\hat{\gamma}$	$\tau + \theta$	$\tau - \theta$	$2\hat{\eta}$
Neuber [6]	G	$\frac{2\nu G}{1-2\nu}$	Ga	$2Gl^2(1+b)$	$2Gl^2(1-b)$	$4Gl^2c$
Kessel [7]	G	$\frac{2\nu G}{1-2\nu}$	$\frac{G}{2}c_1$	$G\bar{L}^2$	$G\bar{L}^2c_2$	$2G\bar{L}^2c_3$
Koiter [8]	G	$\frac{2\nu G}{1-2\nu}$		$2Gl^2(1+\eta)$	$2Gl^2(1-\eta)$	
Eringen [9,10]	$\bar{\mu} + \frac{K}{2}$	λ	$\frac{1}{2}K$	$\frac{1}{2}(\bar{\gamma} + \bar{\beta})$	$\frac{1}{2}(\bar{\gamma} - \bar{\beta})$	$\bar{\alpha}$
Schaefer [11]	G	$\frac{2\nu G}{1-2\nu}$	$G\eta_1$	$L^2\frac{G}{12}$	$L^2\frac{G}{12}\eta_2$	$L^2\frac{G}{6}\eta_3$

Note that the relations between the moduli γ , ε and Koiter constants l^2 and η assume the following form, cf Table 1

$$\begin{aligned} \gamma &= 2Gl^2(1+\eta) = 2\mu l^2(1+\eta) \\ \varepsilon &= 2Gl^2(1-\eta) = 2\mu l^2(1-\eta) \end{aligned}$$

and hence we obtain

$$l^2 = \frac{\gamma + \varepsilon}{4\mu} \quad \eta = \frac{\gamma - \varepsilon}{\gamma + \varepsilon} \quad (2.3)$$

Further on we shall omit the body forces. The equilibrium equations assume the form

$$\sigma^{ji}_{,j} = 0 \quad \epsilon^{ijk} \sigma_{jk} + \mu^{ji}_{,j} = 0 \quad (2.4)$$

The same equations expressed in terms of displacement and rotation fields read

$$(1 + \kappa) \bar{\nabla}^2 \mathbf{u} + \left(\frac{1}{1 - 2\nu} - \kappa \right) \text{grad div } \mathbf{u} + 2\kappa \text{rot } \phi = 0 \quad (2.5)$$

$$(\gamma + \varepsilon) \bar{\nabla}^2 \phi + (\beta + \gamma - \varepsilon) \text{grad div } \phi + 2\alpha (\text{rot } \mathbf{u} - 2\phi) = 0$$

Here ν represents Poisson's ratio. The κ constant is given by

$$\kappa = \frac{\alpha}{\mu} \quad (2.6)$$

The Laplace operator in R^3 has been denoted by $\bar{\nabla}^2$.

3. Biharmonic representation

Let us consider an elastic layer of thickness h , freed from loads on the faces $x^3 = z = \pm h/2$. To find the solution to Eqs (2.5) that fulfils the homogeneous boundary conditions on the faces

$$\sigma_{3i} \left(x^\beta, \pm \frac{h}{2} \right) = 0 \quad (3.1)$$

$$\mu_{3i} \left(x^\beta, \pm \frac{h}{2} \right) = 0$$

we adopt a semi-inverse method.

Let us represent the components of the displacement vector (u_i) and the vector of infinitesimal rotation (ϕ_i) in the form

$$u_\alpha(x^\beta, z) = t(z)v(x^\beta)_{,\alpha} + s(z)\nabla^2 v(x^\beta)_{,\alpha} \quad (3.2)$$

$$u_3(x^\beta, z) = g(z)v(x^\beta) + f(z)\nabla^2 v(x^\beta)$$

$$\phi_\alpha(x^\gamma, z) = \epsilon_\alpha^\beta \left(R_1(z)v(x^\gamma)_{,\beta} + R_2(z)\nabla^2 v(x^\gamma)_{,\beta} \right) \quad (3.3)$$

$$\phi_3 = 0$$

where $t(z)$, $s(z)$, $g(z)$, $f(z)$, $R_1(z)$ and $R_2(z)$ are unknown functions which satisfy the following conditions

$$\begin{aligned} t(z) &= -t(-z) & s(z) &= -s(-z) \\ g(z) &= g(-z) & f(z) &= f(-z) \\ R_1(-z) &= R_1(z) & R_2(-z) &= R_2(z) \end{aligned} \quad (3.4)$$

On inserting (3.2) and (3.3) into the set of equations (2.5) one concludes that there exist non-trivial solutions to this system, provided the function $v(x^\alpha)$ satisfies Eq (1.1) and the unknown functions in z satisfy the following system of ordinary differential equations

$$\begin{aligned} g'' &= 0 \\ (1 + \kappa)g + \frac{2(1 - \nu)}{1 - 2\nu} f'' + \left(\frac{1}{1 - 2\nu} - \kappa \right) t' - 2\kappa R_1 &= 0 \\ (1 + \kappa)t'' + \left(\frac{1}{1 - 2\nu} - \kappa \right) g' + 2\kappa R_1' &= 0 \\ (1 + \kappa)s'' + \frac{2(1 - \nu)}{1 - 2\nu} t + \left(\frac{1}{1 - 2\nu} - \kappa \right) f' + 2\kappa R_2' &= 0 \\ R_1'' - (1 + \kappa)k^2 R_1 + \frac{1}{2}(1 + \kappa)k^2 (g - t') &= 0 \\ R_1 + R_2'' - (1 + \kappa)k^2 R_2 - \frac{1}{2}(1 + \kappa)k^2 (s' - f) &= 0 \end{aligned} \quad (3.5)$$

where $(\cdot)' = \frac{d(\cdot)}{dz}$ and the k constant is defined by

$$k^2 = \frac{N^2}{l^2} \quad N^2 = \frac{\kappa}{1 + \kappa} \quad (3.6)$$

The coefficient N is nondimensional with the value lying within the interval $[0, 1]$.

The solution to the system (3.5) which satisfies the boundary conditions (3.1) can be cast in the following form

$$\begin{aligned} t(z) &= -zC_1 \\ s(z) &= -\frac{(2 - \nu)h^2}{24(1 - \nu)} z \left(C_2 - C_1 \frac{4z^2}{h^2} \right) - l^2 h C_1 \frac{\sinh kz}{\sinh \frac{kh}{2}} \\ g(z) &= R_1(z) = C_1 \\ f(z) &= -\frac{h^2}{24(1 - \nu)} \left[6 \left(1 - \frac{2\nu z^2}{h^2} \right) C_1 - (2 - \nu) C_2 \right] \\ R_2(z) &= -\frac{h^2}{24(1 - \nu)} \left(3C_1 - (2 - \nu) C_2 + 12(1 - \nu) \frac{z^2}{h^2} C_1 - \frac{12(1 - \nu) \cosh kz}{kh \sinh \frac{kh}{2}} C_1 \right) \end{aligned} \quad (3.7)$$

The constants C_1 and C_2 determine the physical meaning of $v(x^\alpha)$. Without any loss of generality the constant C_1 can be fixed as equal to unity, cf [1].

Let us substitute (3.7) into (3.2) and (3.3) and assume $C_1 = 1$. Then one arrives at the following representation for displacement and rotation fields

$$u_\alpha(x^\beta, z) = -\left\{zv(x^\beta)_{,\alpha} + \left[\frac{(2-\nu)h^2}{24(1-\nu)}z\left(C_2 - \frac{4z^2}{h^2}\right) + l^2h\frac{\sinh kz}{\sinh \frac{kh}{2}}\right]\nabla^2v(x^\beta)_{,\alpha}\right\} \quad (3.8)$$

$$u_3(x^\beta, z) = v(x^\beta) - \frac{h^2}{24(1-\nu)}\left[6\left(1 - \frac{2\nu z^2}{h^2}\right) - (2-\nu)C_2\right]\nabla^2v(x^\beta)$$

$$\phi_\alpha(x^\gamma, z) = \epsilon_\alpha^\beta\left[v(x^\gamma)_{,\alpha} + \frac{h^2}{24(1-\nu)}\left((2-\nu)C_2 - 3 - 12(1-\nu)\frac{z^2}{h^2} + \frac{12(1-\nu)\cosh kz}{kh\sinh \frac{kh}{2}}\right)\nabla^2v(x^\gamma)_{,\alpha}\right] \quad (3.9)$$

$$\phi_3 = 0$$

On using formulae (2.1), (2.2), (3.8) and (3.9) one obtains expressions defining the stress and couple-stress components

$$\sigma_{\alpha\beta}(x^\gamma, z) = -\frac{2\mu}{1-\nu}\left\{z\left((1-\nu)v_{,\alpha\beta} + \nu\nabla^2v\delta_{\alpha\beta} + \left[\frac{(2-\nu)h^2}{24}z\left(C_2 - \frac{4z^2}{h^2}\right) + (1-\nu)l^2h\frac{\sinh kz}{\sinh \frac{kh}{2}}\right]\nabla^2v(x^\gamma)_{,\alpha\beta}\right\} \quad (3.10)$$

$$\sigma_{\alpha 3}(x^\beta, z) = -\frac{\mu h^2}{4(1-\nu)}\left[\left(1 - \frac{4z^2}{h^2}\right) + 8(1-\nu)\frac{kl^2\cosh kz}{h\sinh \frac{kh}{2}}\right]\nabla^2v(x^\beta)_{,\alpha}$$

$$\begin{aligned} \mu_{\alpha\beta}(x^\delta, z) = & 4\mu l^2\epsilon_\beta^\gamma\left\{v_{,\gamma\alpha} + \left[\frac{h\cosh kz}{2k\sinh \frac{kh}{2}} - \frac{h^2}{24(1-\nu)}\left(3 + 12(1-\nu)\frac{z^2}{h^2} - \right.\right. \right. \\ & \left.\left.\left. -(2-\nu)C_2\right)\right]\nabla^2v_{,\gamma\alpha}\right\} + 4\mu l^2\eta\epsilon_\alpha^\gamma\left\{v_{,\gamma\beta} + \right. \\ & \left. + \left[\frac{h\cosh kz}{2k\sinh \frac{kh}{2}} - \frac{h^2}{24(1-\nu)}\left(3 + 12(1-\nu)\frac{z^2}{h^2} - (2-\nu)C_2\right)\right]\nabla^2v_{,\gamma\beta}\right\} \end{aligned} \quad (3.11)$$

$$\sigma_{3\alpha}(x^\beta, z) = -\frac{\mu h^2}{4(1-\nu)}\left(1 - \frac{4z^2}{h^2}\right)\nabla^2v_{,\alpha} \quad (3.12)$$

$$\sigma_{33}(x^\alpha, z) = 0 \quad \mu_{33}(x^\alpha, z) = 0 \quad (3.13)$$

$$\mu_{3\alpha} = -2\mu l^2 h \epsilon_{\alpha}^{\beta} \left(2 \frac{z}{h} - \frac{\sinh kz}{\sinh \frac{kh}{2}} \right) \nabla^2 v_{,\beta} \quad (3.14)$$

$$\mu_{\alpha 3} = \eta \mu_{3\alpha}$$

It is readily seen that if the function v fulfils the Eq (1.1), then all differential equations (2.4), (2.5) and boundary conditions (3.1) are satisfied. In their general form (3.8) \div (3.14) these equations have not been up till now reported in the literature.

The C_2 constant can be chosen so as to assign a clear physical meaning to the function $v(x^\alpha)$.

1. For $C_2 = 3$ the $v(x^\alpha)$ function represents deflection of the layer faces

$$\hat{w}(x^\alpha) \stackrel{\text{df}}{=} u_3(x^\alpha, \pm \frac{h}{2})$$

2. for $C_2 = \frac{6}{2-\nu}$ this function stands for the mid-plane deflection

$$w(x^\alpha) \stackrel{\text{df}}{=} u_3(x^\alpha, 0)$$

3. at $C_2 = \frac{6-\nu}{2-\nu}$ this function represents a common mean value

$$\bar{w}(x^\alpha) \stackrel{\text{df}}{=} \frac{1}{h} \int_{-h/2}^{h/2} u_3(x^\alpha, z) dz$$

4. at $C_2 = \frac{3(10-\nu)}{5(2-\nu)}$ we obtain a weighted mean value (cf [1])

$$\tilde{w}(x^\alpha) \stackrel{\text{df}}{=} \frac{3}{2h} \int_{-h/2}^{h/2} \left(1 - 4 \frac{z^2}{h^2} \right) u_3(x^\alpha, z) dz$$

Thus the representations for displacements, stresses and stress resultants can be expressed in terms of different scalar functions (\hat{w} , w , \bar{w} , \tilde{w} , etc.) standing for the deflection of the layer.

Let us compute the quantity $\phi = \frac{1}{2} \text{rot} u$. On using (3.8) we obtain

$$\begin{aligned} \varphi_\alpha(x^\gamma, z) = & \epsilon_{\alpha}^{\beta} \left[v(x^\gamma)_{,\beta} + \frac{h^2}{24(1-\nu)} \left((2-\nu)C_2 - 3 - \frac{12(1-\nu)z^2}{h^2} + \right. \right. \\ & \left. \left. + \frac{12l^2(1-\nu)k \cosh kz}{h \sinh \frac{kh}{2}} \right) \nabla^2 v(x^\gamma)_{,\beta} \right] \quad (3.15) \end{aligned}$$

$$\varphi_3 = 0$$

It is readily seen that the components of the averaged - rotation vector (φ_α) do not coincide with the components of the infinitesimal vector (ϕ_α).

4. Passages to the limits

The following passage to a limit transforms the displacement vector representation for the Cosserat layer to the representation for the layer made of the Grioli-Toupin (G-T) material [6,12,13]

(GPSS in the G-T material) = $\lim_{\kappa \rightarrow \infty}$ (GPSS for the Cosserat material)

Passing in (3.6) with κ to infinity one finds

$$N^2 = 1 \qquad k^2 = \frac{1}{l^2} \qquad (4.1)$$

Substituting equality (4.1) into (3.8) and (3.9) one obtains

$$u_\alpha(x^\beta, z) = -\left\{zv(x^\beta)_{,\alpha} + \left[\frac{(2-\nu)h^2}{24(1-\nu)}z\left(C_2 - \frac{4z^2}{h^2}\right) + l^2h\frac{\sinh\frac{z}{l}}{\sinh\frac{h}{2l}}\right]\nabla^2v(x^\beta)_{,\alpha}\right\} \qquad (4.2)$$

$$u_3(x^\beta, z) = v(x^\beta) - \frac{h^2}{24(1-\nu)}\left[\left(6 - \frac{12\nu z^2}{h^2}\right) - (2-\nu)C_2\right]\nabla^2v(x^\beta)$$

$$\begin{aligned} \phi_\alpha(x^\gamma, z) = \varphi_\alpha(x^\gamma, z) = \epsilon_\alpha{}^\beta\left\{v(x^\gamma)_{,\alpha} + \left[\frac{h^2}{24(1-\nu)}\left((2-\nu)C_2 - 3 - \right.\right.\right. \\ \left.\left.\left.- 12(1-\nu)\frac{z^2}{h^2}\right) + \frac{1}{2}lh\frac{\cosh\frac{z}{l}}{\sinh\frac{h}{2l}}\right]\nabla^2v(x^\gamma)_{,\alpha}\right\} \end{aligned} \qquad (4.3)$$

$$\varphi_3 = 0$$

The representation given above concerns the displacement field in a medium with constrained rotations [1]. Under the assumptions (4.1) the stresses given by (3.10) ÷ (3.14) describe the GPSS in the plate made of a Grioli-Toupin material (cf [1]).

Similar representations for the Hookean material can be arrived at by passing to zero with l in the formulae (3.8) ÷ (3.14) or (4.2). Such representations for displacements and stresses turn out to coincide with those found previously (cf [1]). The couple-stresses become zero and the infinitesimal rotation ϕ becomes equal to the averaged rotation φ .

Let us compute the limits of the expressions (3.8) ÷ (3.14) for $\alpha \rightarrow 0$, i.e. at $N = 0$. In the micropolar elasticity this case is viewed as a pathological one [14].

If $N = 0$, in many problems of micropolar elasticity the solutions do not tend to classical elasticity solutions. In the problem considered here we just face this situation. Obtained via passing to zero with N the expressions for the stresses satisfy the equilibrium equations (2.4)₁ (provided that Eq (1.1) is satisfied) but the couple-stresses $\mu_{\alpha\beta}$ become indeterminate and the equilibrium equations (2.4) turn out to be violated. This is a consequence of the fact that at $N = 0$ the components ϕ_α tend to infinity.

Finally let us note that in the GPSS considered the classical (i.e. symmetric) elasticity solution [1] can be obtained if one assumes $l \rightarrow 0$ ($k \rightarrow \infty$) in Eqs (3.8) \div (3.14).

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Reprezentacja biharmoniczna w rozwiązywaniu problemów równowagi płyty wykonanej z materiału Cosseratów

Streszczenie

W pracy wyznaczono przedstawienie wektora przemieszczenia i infinitezimalnego obrotu, opisujące uogólniony płaski stan naprężenia w płycie Cosseratów. Przedstawiona reprezentacja wektora przemieszczenia prowadzi do rozwiązania równania biharmonicznego na funkcję przedstawiającą ugięcie.

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