

VIBRO-ACOUSTIC ANALYSIS OF LAMINATED DOUBLE GLAZING USING THE FORCE IDENTIFICATION METHOD

MOUNIR BEN JDIDIA, ALI AKROUT, DHOUBA TOUNSI, TAHAR FAKHFAKH,
MOHAMED HADDAR

*Mechanics, Modelling and Production Research Laboratory, Mechanical Engineering Department, National School
of Engineers of Sfax, Sfax, Tunisia*

*e-mail: mounir.benjdida@isetsf.rnu.tn; ali.akrout@enit.rnu.tn and ali_akrout2005@yahoo.fr; dhouha.ing@gmail.com;
tahar.fakhfakh@enis.rnu.tn; mohamed.haddar@enis.rnu.tn*

This paper presents a procedure for identifying wave forms and excitation frequencies of some forces applied on a given complex fluid-structure coupled system by using only its vibro-acoustic response. The considered concept is called the Independent Component Analysis (ICA) which is based on the Blind Source Separation (BSS). In this work, the ICA method is exploited in order to determine the excitation force applied to a thin-film laminated double glazing system enclosing a thin fluid cavity and limited by an elastic joint. The dynamic response of the studied fluid-structure coupled system is determined by finite element discretization and minimization of the homogenized energy functional of the coupled problem. This response will serve as the input for the ICA algorithm in order to extract the applied excitation.

Keywords: fluid-structure interaction, thin-film laminated plate, ICA, excitation force, Kurtosis

1. Introduction

Laminated and sandwich plates present their advantage when they are used to reduce noise and vibration due to their high structural damping. In fact, the presence of viscoelastic core or ultra-thin film gives more rigidity to laminates with a much reduced vibration deflection.

That is why the resolution of direct fluid-structure coupled problems, such as the study of acoustic transparency of double panel systems, has been carried out in several research works such as those developed by Cheng *et al.* (2005), Abdennadher *et al.* (2005) and Akrout *et al.* (2010).

In this work, we deal with a system composed of a thin-film laminated double glazing system enclosing a thin fluid cavity and limited by an elastic joint, to which we use the ICA concept in order to extract the applied force.

In fact, the Blind Source Separation (BSS) is an important research area in signal processing and data analysis.

The first formulation of the problem was made in 1985 by researchers in neuroscience and signal processing to model biologically coding of motion. In fact, the source separation problem was developed by Héroult and Ans (1984) and Héroult *et al.* (1985). Then, Comon (1994) made the link between the Independent Component Analysis (ICA) and the Blind Source Separation (BSS).

The independent component analysis (ICA) is one of the major pathways of sources separation concept (Hyvärinen and Oja, 2000; Antoni, 2005; Zarzoso and Comon, 2008; Abbes *et al.*, 2011; Akrout *et al.*, 2012b). It extracts from the observed signal components as independent as possible. In the recent years, this method (ICA) was investigated for extracting signals such as

excitation forces and internal defaults in mechanical systems (Akrouit *et al.*, 2012b; Taktak *et al.*, 2012).

In this work, dynamical study is carried out in order to model the vibratory excitation of a vibro-acoustic problem defined by a thin fluid cavity coupled to the thin-film laminated glass plate structural model developed in our previous work (Akrouit *et al.*, 2012a). Then, the ICA concept is applied to the finite element signals defined by the displacement vector of the studied system in order to extract the wave form and the excitation frequencies of the external applied forces. So, the main original contribution of this work is based on the developed fluid-structure laminated double glazing model which can be exploited for identifying excitation sources by the inverse method (ICA).

2. Description of the studied fluid-structure coupled system

The studied system is composed of two ultra-thin film laminated glass plates coupled to a thin fluid cavity and related with an elastic joint, as presented in Fig. 1. k_0 , k_1 and k_2 represent the laminate edge stiffness and F_0 is the harmonic uniform distributed force applied to thin-film laminated plate 1.

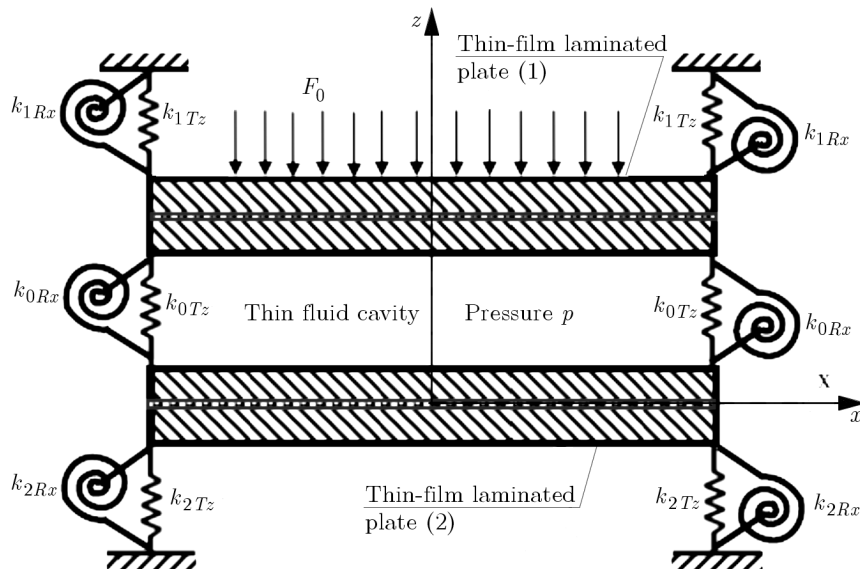


Fig. 1. Ultra-thin film laminated double glazing system (the xz -plane)

3. Resolution of the direct vibro-acoustic problem

3.1. Dynamic equation of the coupled problem

Discretization by the finite element method and minimization of the coupled system energy functional give the following coupled matrix system (Akrouit *et al.*, 2010, 2012a)

$$\begin{bmatrix} \mathbf{K}_1 + \mathbf{J}_1 + \mathbf{J}_0 - \omega^2 \mathbf{M}_1 & -\mathbf{J}_{012} & -\mathbf{C}_1 \\ -\mathbf{J}_{012}^T & \mathbf{K}_2 + \mathbf{J}_2 + \mathbf{J}_0 - \omega^2 \mathbf{M}_2 & \mathbf{C}_2 \\ -\mathbf{C}_1^T & \mathbf{C}_2^T & \frac{h_f}{\rho_f \omega^2} (\mathbf{H} - k_f^2 \mathbf{Q}) \end{bmatrix} \begin{Bmatrix} \mathbf{U}_1 \\ \mathbf{U}_2 \\ \mathbf{P} \end{Bmatrix} = \begin{Bmatrix} \mathbf{F}^{ext} \\ \mathbf{0} \\ \mathbf{0} \end{Bmatrix} \quad (3.1)$$

where $\mathbf{K}_1 + \mathbf{J}_1 + \mathbf{J}_0$, $\mathbf{K}_2 + \mathbf{J}_2 + \mathbf{J}_0$ and \mathbf{J}_{012} are the stiffness matrices of the structural part of the coupled system. \mathbf{M}_1 and \mathbf{M}_2 are the mass matrices of the laminates. \mathbf{C}_1 and \mathbf{C}_2 are the fluid-

-structure coupling matrices. \mathbf{H} and \mathbf{Q} represent the acoustic matrices. h_f , ρ_f and $k_f = \omega/c_f$ represent the cavity thickness, the fluid density and the acoustic wave number, respectively. c_f and ω are the speed of sound and the angular frequency, respectively. \mathbf{U}_1 , \mathbf{U}_2 and \mathbf{P} are the nodal response vectors. $\mathbf{F}^{ext} = \mathbf{F}_0 \exp(-i\omega t)$ represent the nodal force vector to be reconstituted by the developed inverse method (ICA).

The film-laminate finite element presents seven degrees of freedom at each node ($u_m, v_m, \mathbf{u}_\tau, \mathbf{v}_\tau, w, \beta_x, \beta_y$), whereas the fluid cavity finite element presents one degree of freedom at each node (pressure p).

3.2. Resolution of the dynamic equation

The resolution of the direct problem defined by equation (3.1) is based on a modal approach (Akrouit *et al.*, 2010, 2012a). Then, the following eigenvalue problems to be solved are considered

$$\begin{aligned} (\mathbf{K}_1 + \mathbf{J}_1 + \mathbf{J}_0 - \omega^2 \mathbf{M}_1) \mathbf{U}_1 &= \mathbf{0} & (\mathbf{K}_2 + \mathbf{J}_2 + \mathbf{J}_0 - \omega^2 \mathbf{M}_2) \mathbf{U}_2 &= \mathbf{0} \\ \frac{h_f}{\rho_f \omega^2} (\mathbf{H} - k_f^2 \mathbf{Q}) \mathbf{P} &= \mathbf{0} \end{aligned} \quad (3.2)$$

By resolving these equations, three modal bases could be constructed: Φ_{s1} for the structure defined by (laminate 1+joint 1+joint 0), Φ_{s2} for the structure (laminate 2+joint 2+joint 0) and Φ_f for the fluid cavity. The second step consists on reducing the size of system (3.1) by modal projection on these modal bases. So, matrix system (3.1) becomes (Akrouit *et al.*, 2010, 2012a)

$$\begin{bmatrix} (\overline{\mathbf{K}}_1 + \overline{\mathbf{J}}_1 + \overline{\mathbf{J}}_0) - \omega^2 \overline{\mathbf{M}}_1 & -\overline{\mathbf{J}}_{012} & -\overline{\mathbf{C}}_1 \\ -\overline{\mathbf{J}}_{012}^T & (\overline{\mathbf{K}}_2 + \overline{\mathbf{J}}_2 + \overline{\mathbf{J}}_0) - \omega^2 \overline{\mathbf{M}}_2 & \overline{\mathbf{C}}_2 \\ -\overline{\mathbf{C}}_1^T & \overline{\mathbf{C}}_2^T & \frac{h_f}{\rho_f \omega^2} (\overline{\mathbf{H}} - k_f^2 \overline{\mathbf{Q}}) \end{bmatrix} \begin{Bmatrix} \overline{\mathbf{U}}_1 \\ \overline{\mathbf{U}}_2 \\ \overline{\mathbf{P}} \end{Bmatrix} = \begin{Bmatrix} \overline{\mathbf{F}}^{ext} \\ \mathbf{0} \\ \mathbf{0} \end{Bmatrix} \quad (3.3)$$

where $(\overline{\mathbf{K}}_i + \overline{\mathbf{J}}_i + \overline{\mathbf{J}}_0) = \Phi_{si}^T (\mathbf{K}_i + \mathbf{J}_i + \mathbf{J}_0) \Phi_{si}$, $\overline{\mathbf{M}}_i = \Phi_{si}^T \mathbf{M}_i \Phi_{si}$ ($i = 1, 2$) are respectively the reduced stiffness and mass matrices of the coupled system. $\overline{\mathbf{J}}_{012} = \Phi_{s1}^T \mathbf{J}_{012} \Phi_{s2}$ is the reduced stiffness matrix due to the structural coupling between laminate 1 and 2. $\overline{\mathbf{H}} = \Phi_f^T \mathbf{H} \Phi_f$ and $\overline{\mathbf{Q}} = \Phi_f^T \mathbf{Q} \Phi_f$ represent the reduced acoustic matrices. $\overline{\mathbf{C}}_i = \Phi_{si}^T \mathbf{C}_i \Phi_f$ is the reduced fluid-laminate ($i = 1, 2$) coupling matrix. $\overline{\mathbf{U}}_1 = \Phi_{s1}^T \mathbf{U}_1$, $\overline{\mathbf{U}}_2 = \Phi_{s2}^T \mathbf{U}_2$ and $\overline{\mathbf{P}} = \Phi_f^T \mathbf{P}$ represent the modal response vectors and $\overline{\mathbf{F}}^{ext} = \Phi_{s1}^T \mathbf{F}^{ext}$ is the modal force vector.

The coupled modal basis $\Phi_c = [\phi_1, \dots, \phi_N]$ (N is the number of retained eigenmodes) which contains the coupled eigenmodes, is obtained from the resolution of the eigenmode reduced coupled problem as presented in our previous works (Akrouit *et al.*, 2010, 2012a).

The modal variables $\alpha_r(\omega)$ of the r -th eigenmode, which are obtained by projecting equation (3.5) on the coupled eigenmode basis Φ_c , could have the following expression (Akrouit *et al.*, 2010)

$$\alpha_r(\omega) = \frac{f_r}{k_r} \left[1 - \left(\frac{\omega}{\omega_r} \right)^2 \right]^{-1} \quad r = 1, 2, \dots, N \quad (3.4)$$

where $\omega_r = \sqrt{k_r/m_r}$ is the r -th eigenfrequency of the coupled system. k_r and m_r are the r -th generalized mass and the r -th generalized stiffness of the coupled system, respectively. f_r is the generalized force of the r -th eigenmode.

So, the dynamic response is determined by modal recombination (Hammami *et al.*, 2005; Akrouit *et al.*, 2010)

$$\mathbf{U}(\omega) = [\phi_1, \dots, \phi_N] \begin{Bmatrix} \alpha_1(\omega) \\ \vdots \\ \alpha_N(\omega) \end{Bmatrix} \quad (3.5)$$

Now, after determining the dynamic response which is defined by the displacement of the studied structure, we will study the inverse problem. In this case, the dynamic response will serve as the input for the ICA algorithm in order to determine the wave form of the applied force signal.

4. The concept of the Independent Component Analysis: ICA

4.1. Definition and principle hypothesis

ICA is a statistical technique that aims to break a random signal multivariate X (measured signal) in a multivariable linear combination of independent signals (the source signals) to highlight the signals as independent as possible from the measured signals.

It was developed by Héroult *et al.* (1985) and it is defined by the following equation

$$\mathbf{X}(t) = \mathbf{A}\mathbf{S}(t) \quad (4.1)$$

where $\mathbf{X}(t)$ and $\mathbf{S}(t)$ are respectively the observed signals through sensors and the source signals, \mathbf{A} is the mixture matrix.

The source separation principle consists of determining a matrix \mathbf{B} in order to estimate N source signals defined by the vector $\mathbf{Y}(t) = [Y_1(t), \dots, Y_N(t)]^T$ as follows (Antoni, 2005; Abbès *et al.*, 2011; Akrouit *et al.*, 2012b)

$$\mathbf{Y}(t) = \mathbf{B}\mathbf{X}(t) \quad (4.2)$$

In order to achieve this goal, general assumptions must be considered (Hyvärinen and Oja, 2000). The principal assumption is the statistical independency of the source signals. The second one imposes non-Gaussian distributions on the source signals (Comon, 1991; Moreau and Macchi, 1993). The last one is defined by the principle of uncorrelated sources. In fact two variables Y_1 and Y_2 are uncorrelated if their covariance is equal to zero. This can be expressed by the following relation

$$E\{Y_1 Y_2\} - E\{Y_1\}E\{Y_2\} = 0 \quad (4.3)$$

4.2. Separation concept

The principle object of the presented method is to extract the source signals from a mixture of the observed signals. In order to achieve this goal, the observed signals of the system should be centred (substrate its mean vector), then whitened (which consist on eliminating the noise, so we obtain a new signal with an uncorrelated component and variance equal to unity). So, the estimated source is defined by Antoni (2005)

$$\mathbf{Y} = \mathbf{W}^H \mathbf{X} \quad (4.4)$$

where \mathbf{W}^H is the separating matrix, $(\cdot)^H$ denotes the conjugate-transpose operator.

In order to guarantee the non-gaussianity of the signals, the estimated sources must maximize the contrast function. The contrast function utilized in the ICA algorithm is the Kurtosis function defined by Zarzoso and Comon (2010). This fourth order cumulant can be normalized as follows

$$K(\omega) = \frac{E\{|y|^4\} - 2E^2\{|y|^2\} - |E\{y^2\}|^2}{E^2\{|y|^2\}} \quad (4.5)$$

Finally, after determining the first column of the separating matrix, the deflation approach is applied in order to extract the corresponding source vector from the original mixture related to the determined column of the separating matrix.

So, each source will be chosen once with the multiplying factor (Hyvärinen and Oja, 2000).

5. Numerical results

The geometrical and physical features of the ultra-thin film laminated glass panel are given as follows (Akrouit *et al.*, 2010):

- two identical skins (glass) for each laminate:
 - Young's modulus $E_1^{p1} = E_2^{p1} = E_1^{p2} = E_2^{p2} = 7.2 \cdot 10^4$ MPa
 - density $\rho_1^{p1} = \rho_2^{p1} = \rho_1^{p2} = \rho_2^{p2} = 2500$ Kg/m³
 - Poisson's ratios $\nu_1^{p1} = \nu_2^{p1} = \nu_1^{p2} = \nu_2^{p2} = 0.22$
 - skin thicknesses for the symmetrical system $h_1^{p1} = h_2^{p1} = h_1^{p2} = h_2^{p2} = 3$ mm
 - skin thicknesses for the asymmetrical system $h_1^{p1} = h_2^{p1} = 3$ mm, $h_1^{p2} = h_2^{p2} = 4$ mm
- film stiffness $k_{film} = 1.362 \cdot 10^7$ N/mm³ (Araldite), $k_{film} = 1.1 \cdot 10^4$ N/mm³ (Epoxy)
- in-plane (x, y) laminate half dimensions $\ell_x = 0.6$ m, $\ell_y = 0.4$ m'

The geometrical and physical parameters of the air cavity are given as follows (Akrouit *et al.*, 2010): $c_f = 340$ m/s, $h_f = 1$ mm, $\rho_f = 1.2$ Kg/m³.

Only the translational joint is considered (Akrouit *et al.*, 2012a): $k_{joint} = 0.264 \cdot 10^{10}$ N/mm².

5.1. Parametric study

Three configurations for the coupled studied system are considered:

- model 1 defined by two identical laminates ($h_1^{p1} = h_2^{p1} = h_1^{p2} = h_2^{p2} = 3$ mm) with an ultra-thin film of Araldite ($k_{film} = 1.362 \cdot 10^7$ N/mm³)
- model 2 characterized by the same laminates as model 1, but another material is chosen for the adhesive film ($k_{film} = 1.1 \cdot 10^4$ N/mm³, Epoxy)
- model 3 distinguished by an asymmetrical double glazing system (laminates: laminate 1: $h_1^{p1} = h_2^{p1} = 3$ mm, laminate 2: $h_1^{p2} = h_2^{p2} = 4$ mm, $k_{film} = 1.362 \cdot 10^7$ N/mm³).

For these three different models, two types of loads are applied on laminate 1: the first one is defined by a uniformly distributed force and the second one is a punctual force.

5.2. Observed signals

For each model defined above, the FE coupled system vibratory responses (transversal displacement on the middle of the first and second laminate: w_1, w_2) are determined and presented in Figs. 2-7.

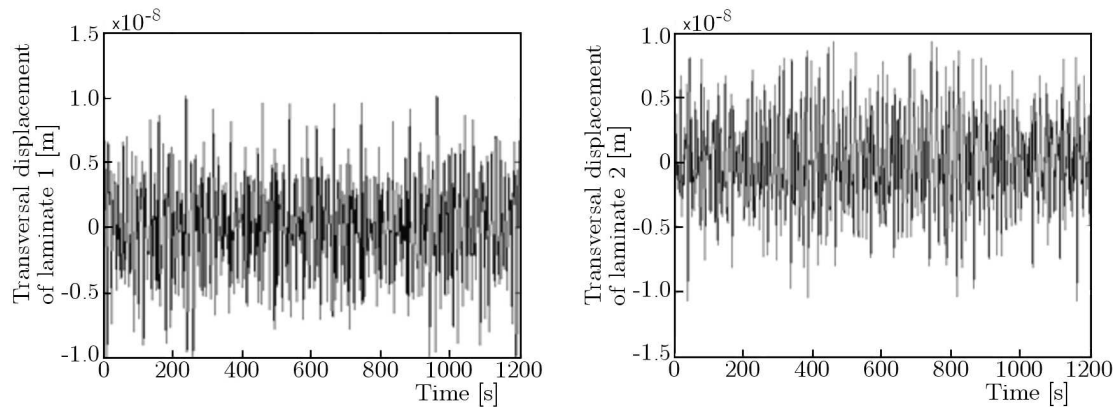


Fig. 2. Model 1: observed signals for a punctual force

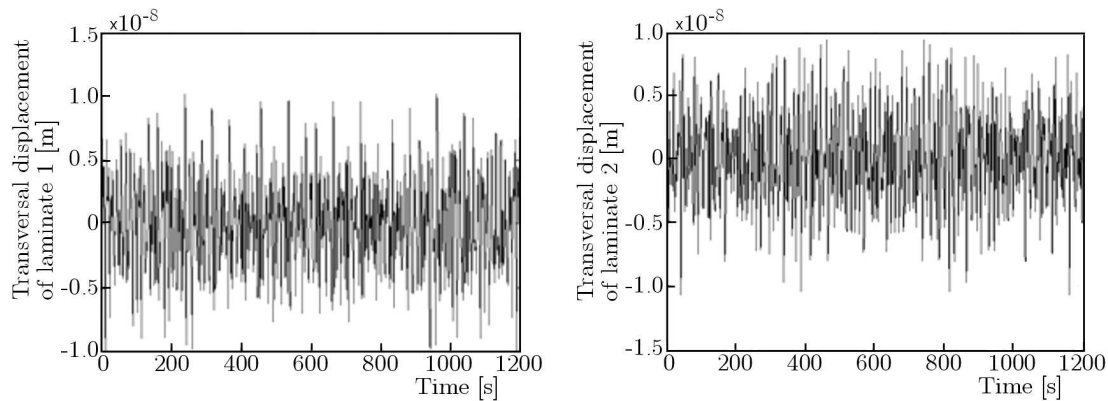


Fig. 3. Model 1: observed signals for a distributed force

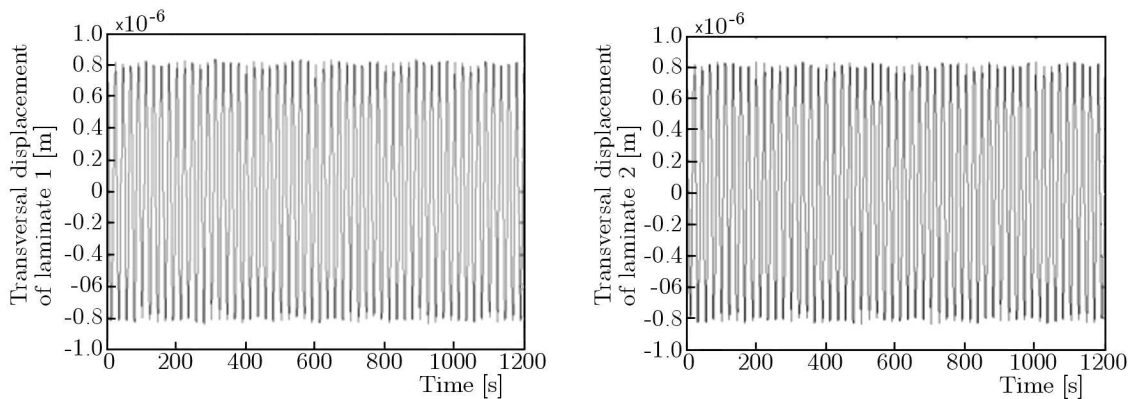


Fig. 4. Model 2: observed signals for a punctual force

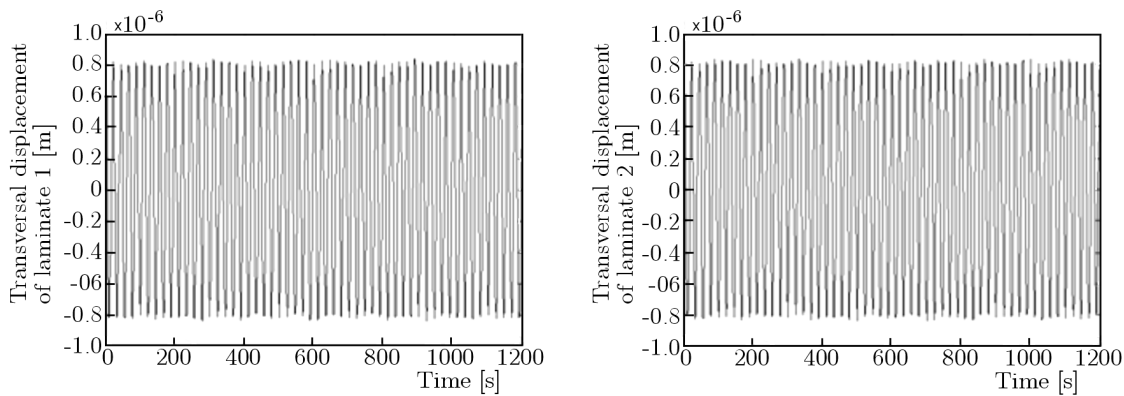


Fig. 5. Model 2: observed signals for a distributed force

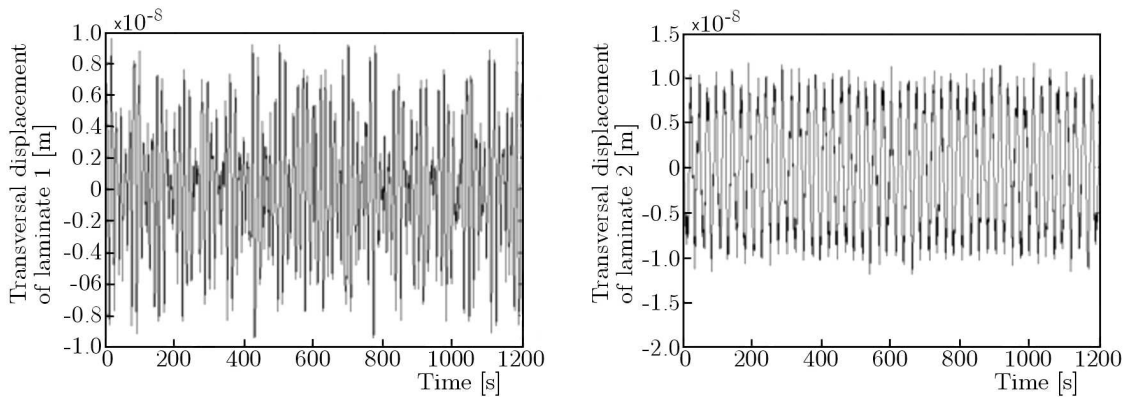


Fig. 6. Model 3: observed signals for a punctual force

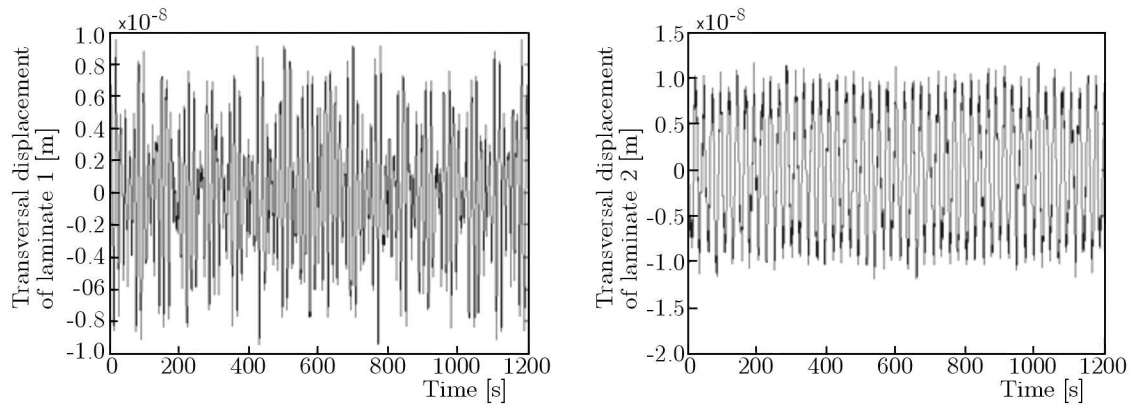


Fig. 7. Model 3: observed signals for a distributed force

Then, after determining the observed signals which represent the displacements in the centre of the first and the second laminate, the obtained results will serve as the input in the ICA algorithm.

5.3. Estimated sources

The wave form and excitation frequency of the punctual and distributed forces applied to the system will be constructed using the ICA algorithm.

The time-evolution of the applied force and the corresponding spectrum (FFT) are presented in Figs. 8a and 8b, respectively. In this case, we have mentioned that this applied excitation can be distributed on the whole nodes of laminate 1. So, it can be also reconstituted by the developed inverse method.

Then, from Fig. 9 to Fig. 14, we present the corresponding ICA results.

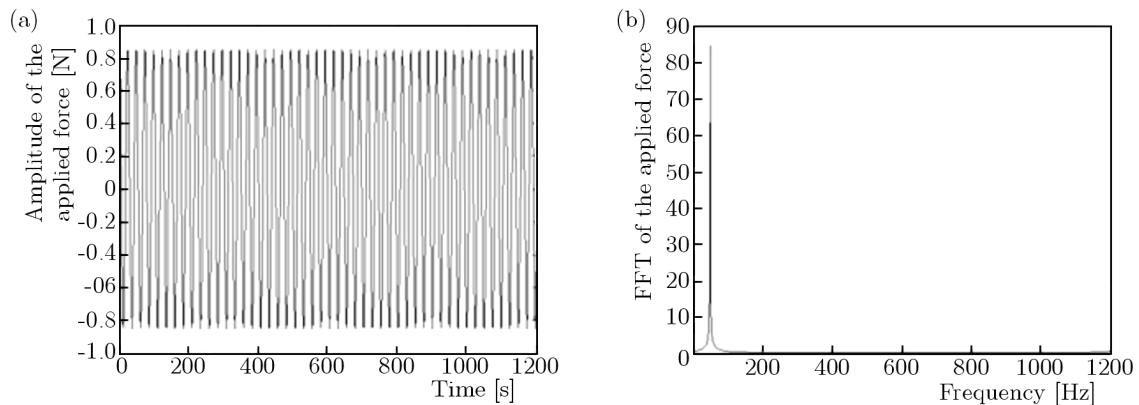


Fig. 8. (a) Time-evolution of the applied excitation source, (b) FFT of the applied excitation source

From Fig. 9 to Fig. 14, we can deduce that the adopted inverse method can be applied to identify the dynamic excitation (the punctual and distributed forces and their spectrum) for analyzing the vibro-acoustic behaviour of a fluid-structure coupled system. In this case, the excitation frequencies of each force are localized and determined.

6. Conclusions

In this paper, one of the major techniques of the Blind Source Separation (BSS) called the Independents Components Analysis (ICA) is presented and exploited in order to extract the

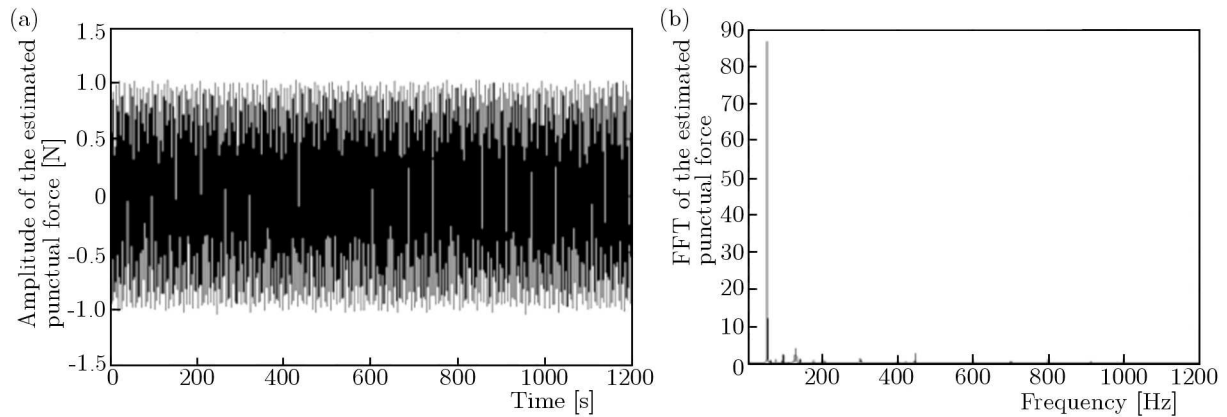


Fig. 9. Model 1: (a) estimated punctual source, (b) FFT of the estimated punctual source

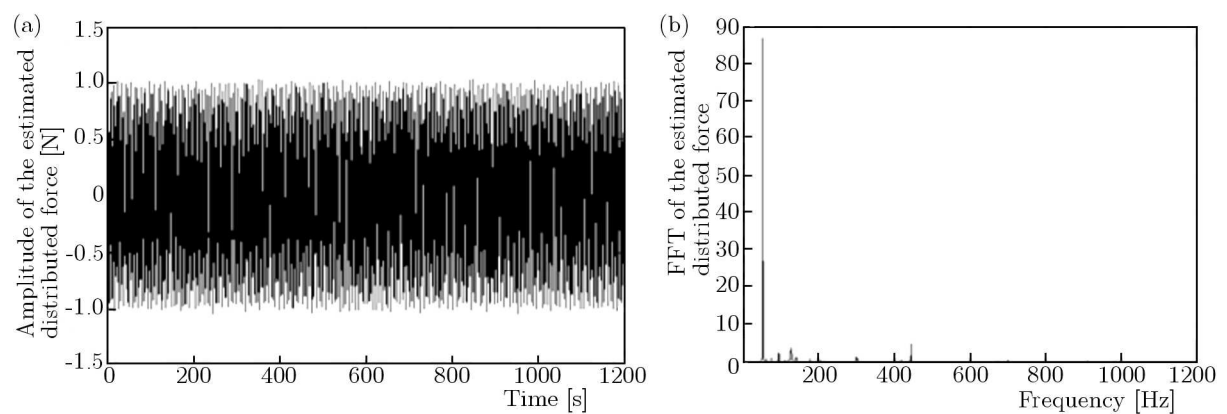


Fig. 10. Model 1: (a) estimated distributed source, (b) FFT of the estimated distributed source

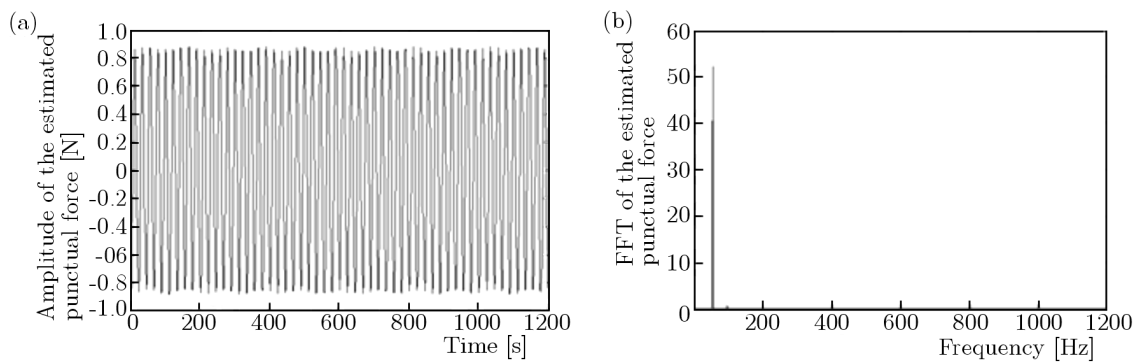


Fig. 11. Model 2: (a) estimated punctual source, (b) FFT of the estimated punctual source

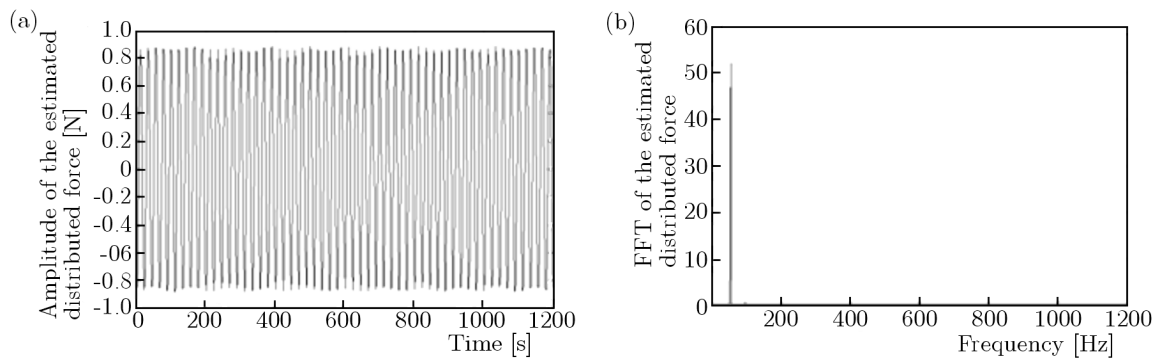


Fig. 12. Model 2: (a) estimated distributed source, (b) FFT of the estimated distributed source

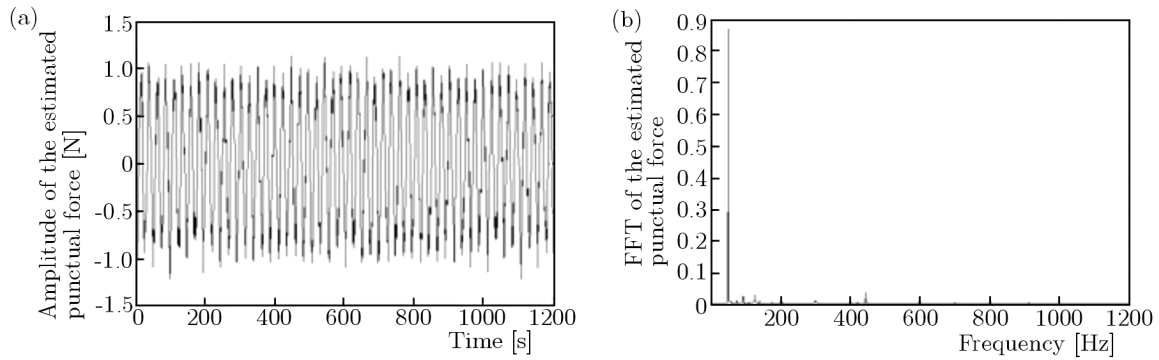


Fig. 13. Model 3: (a) estimated punctual source, (b) FFT of the estimated punctual source

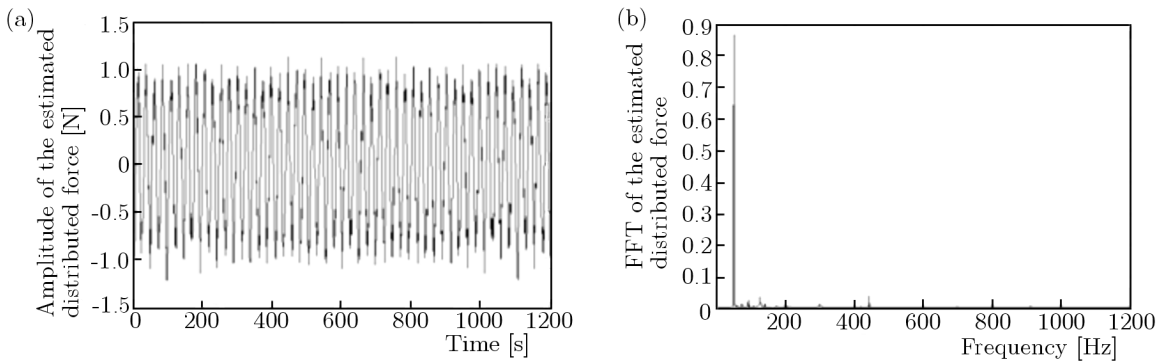


Fig. 14. Model 3: (a) estimated distributed source, (b) FFT of the estimated distributed source

force applied to a fluid-structure coupled system composed of a thin-film laminated double glazing system enclosing a thin fluid cavity and limited by an elastic joint. The vibro-acoustic responses are determined by the modal recombination method which is applied to the Finite Element (FE) coupled matrix system.

As a continuation of our previous published works, this method allows us to determine the wave form of any external or internal forces applied to the structure, so it is a useful method to study complex fluid-structure coupled systems.

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